

# Structured Electronic Design

## Amplifiers: Modeling of Ideal Behavior

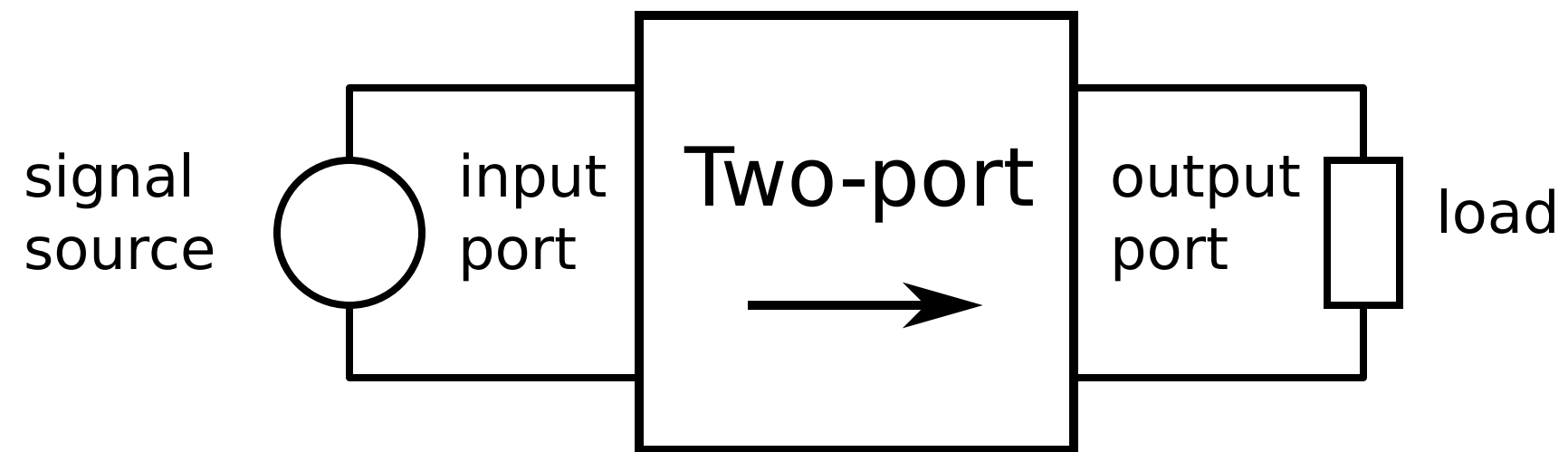
# Two-port model

# Two-port model

Functional model:  
the power port will be omitted

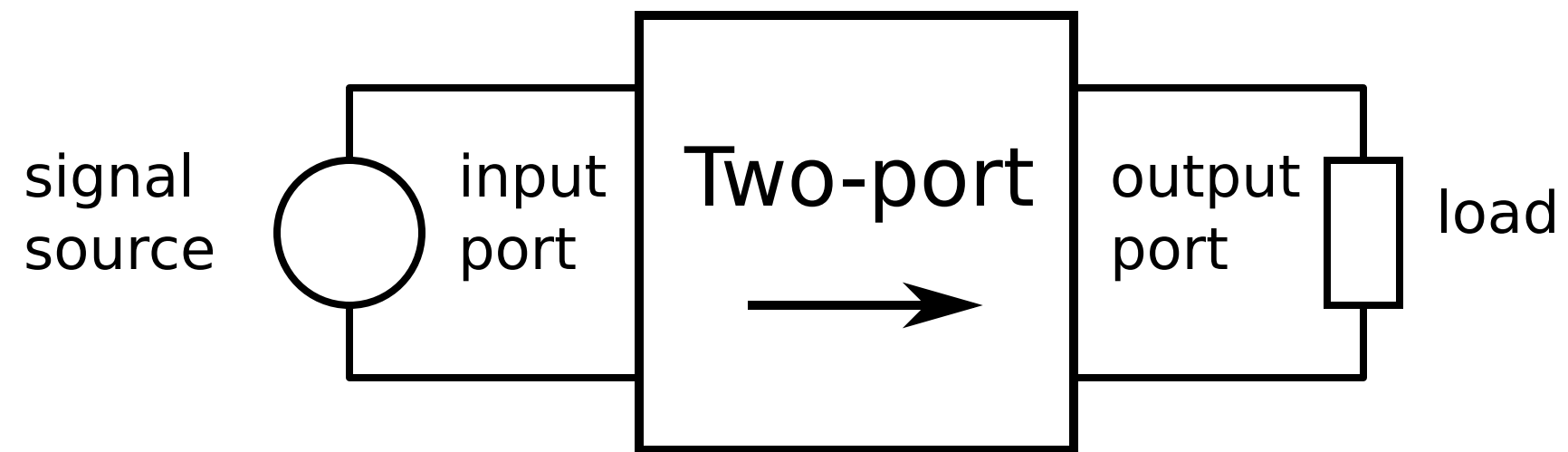
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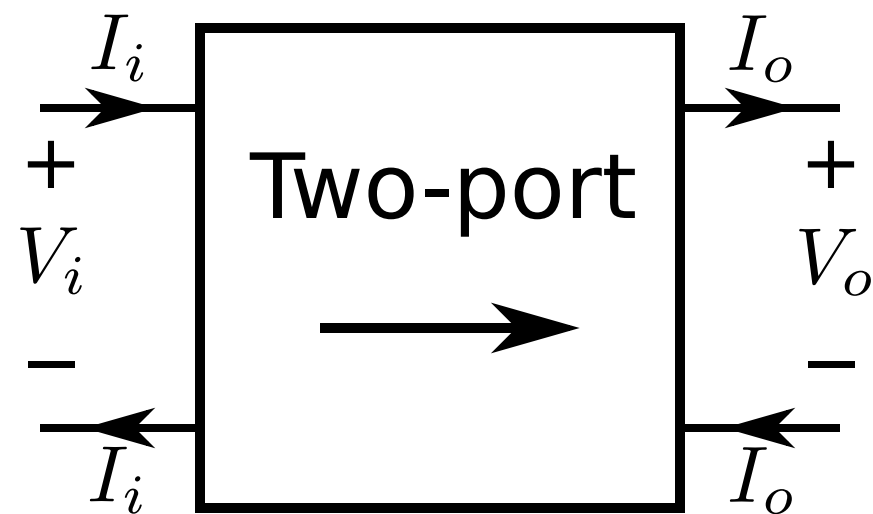


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## Two-port modeling: Chapter 18.6



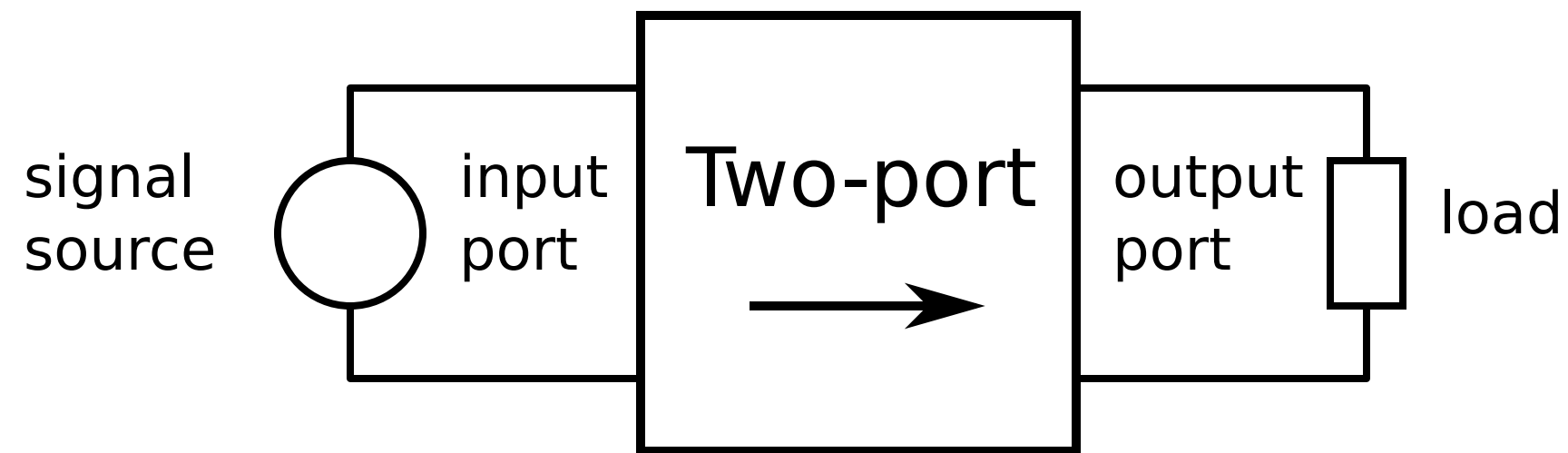
Two-port  
conditions

Two-port  
representations

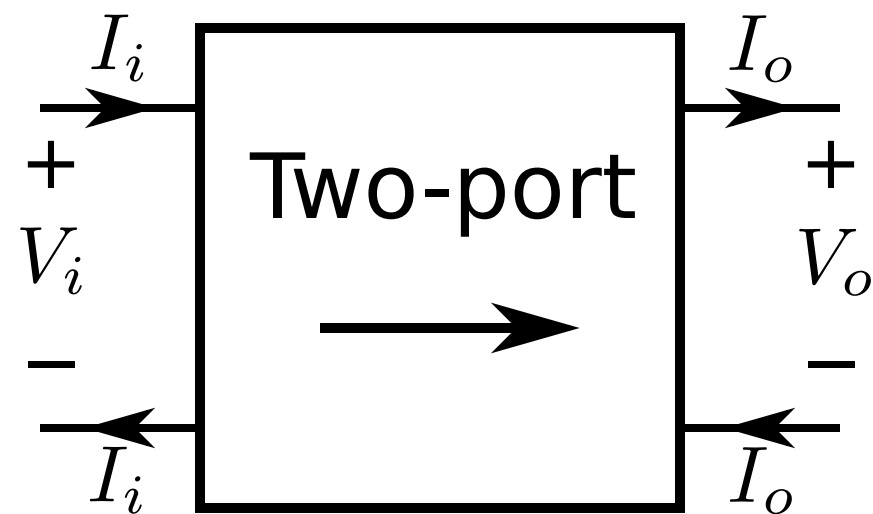
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Functional model:  
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Transmission-1 (anti-causal)  
representation



Two-port modeling: Chapter 18.6

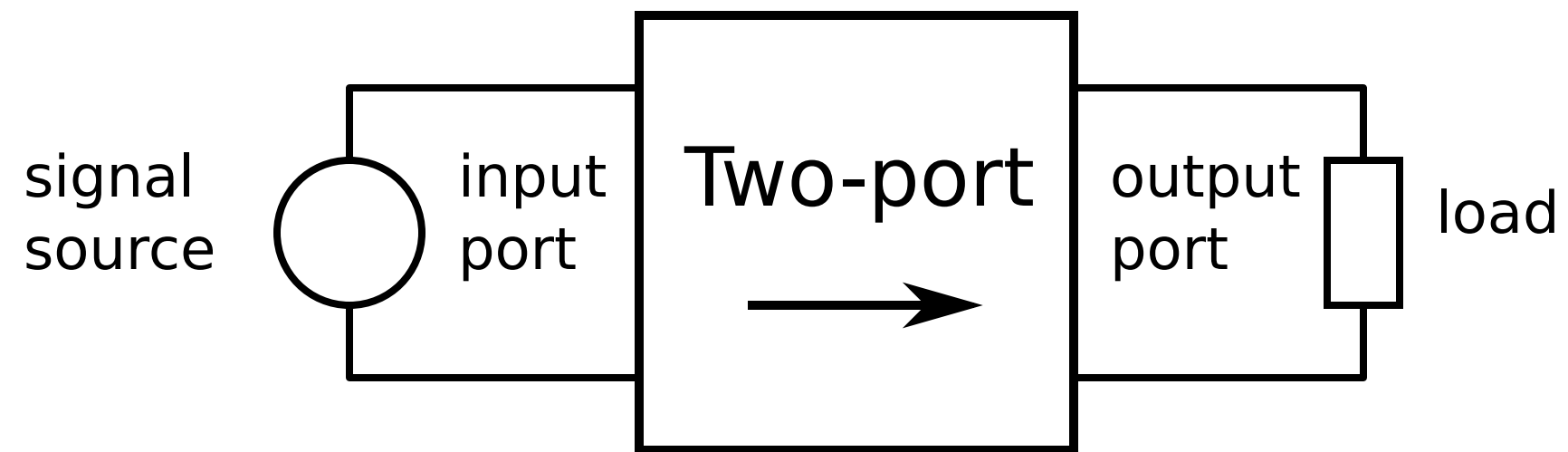


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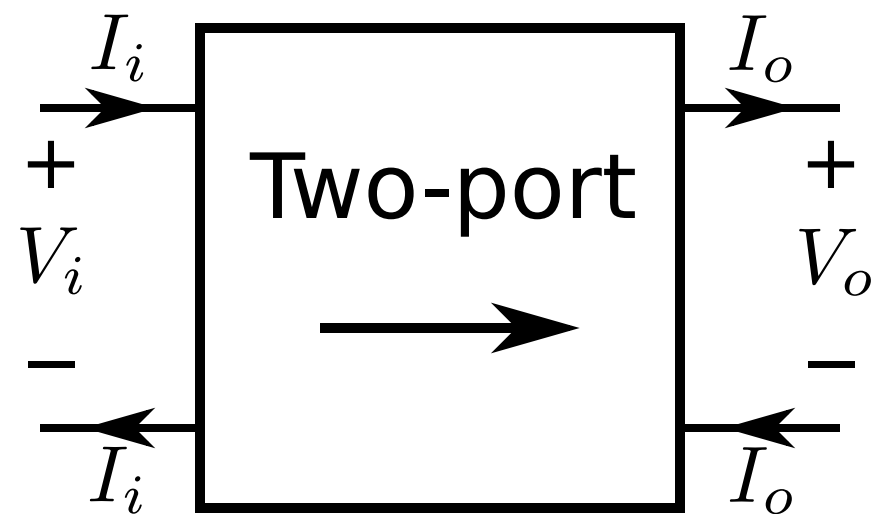
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Transmission-1 (anti-causal)  
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$$\begin{pmatrix} V_i \\ I_i \end{pmatrix} = \begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} V_o \\ I_o \end{pmatrix}$$

Two-port modeling: Chapter 18.6

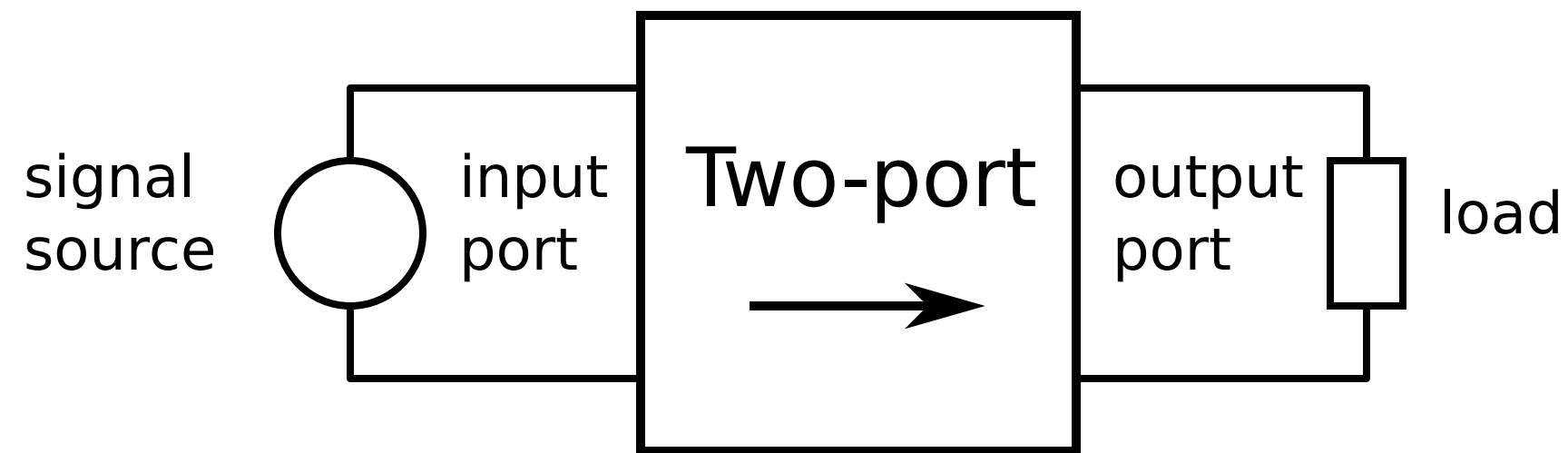


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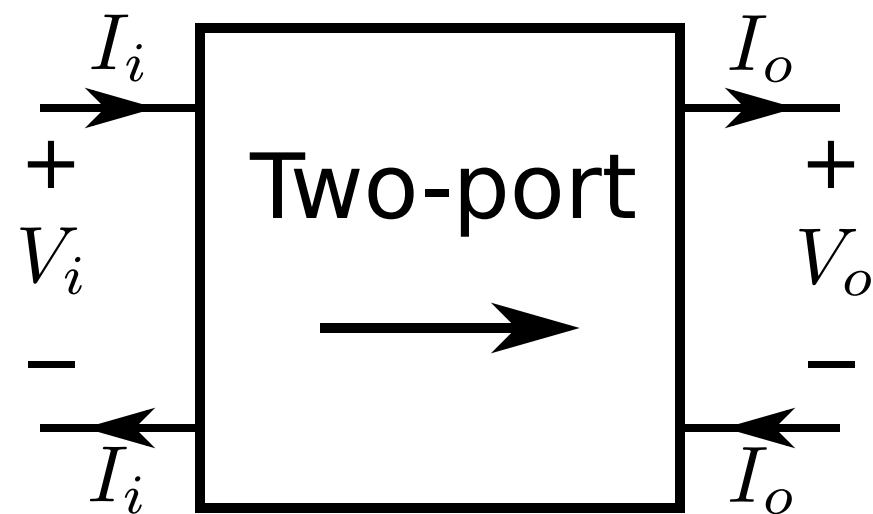
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Two-port modeling: Chapter 18.6



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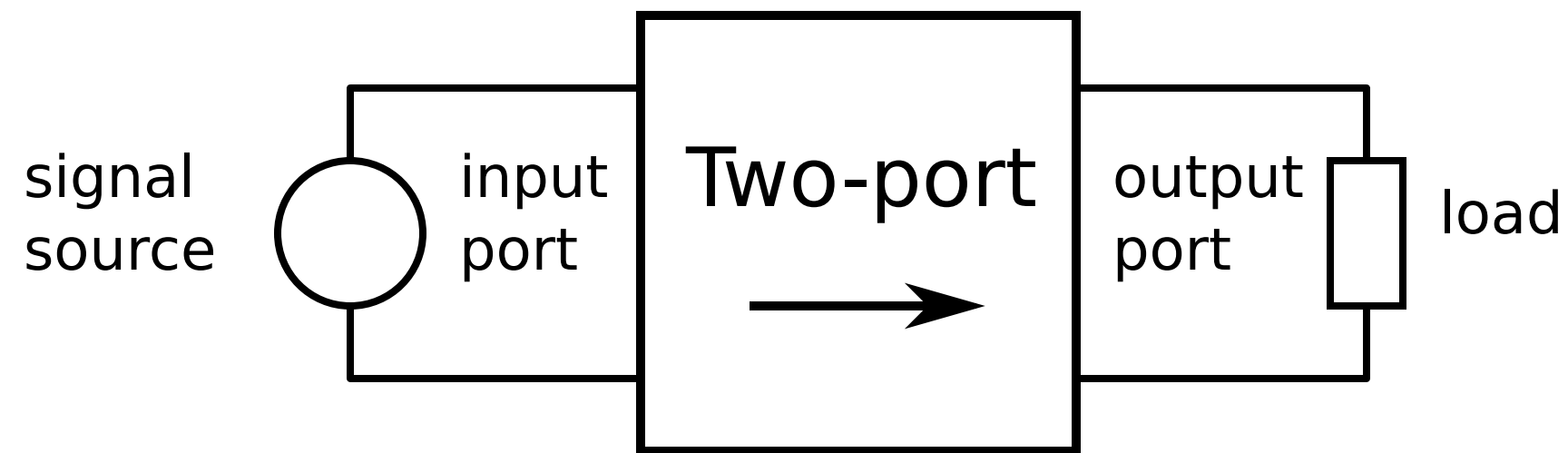
$$\begin{pmatrix} V_i \\ I_i \end{pmatrix} = \begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} V_o \\ I_o \end{pmatrix}$$

$$A = \frac{1}{\mu} = \left. \frac{V_i}{V_o} \right|_{I_o=0}, \quad \text{Open output}$$

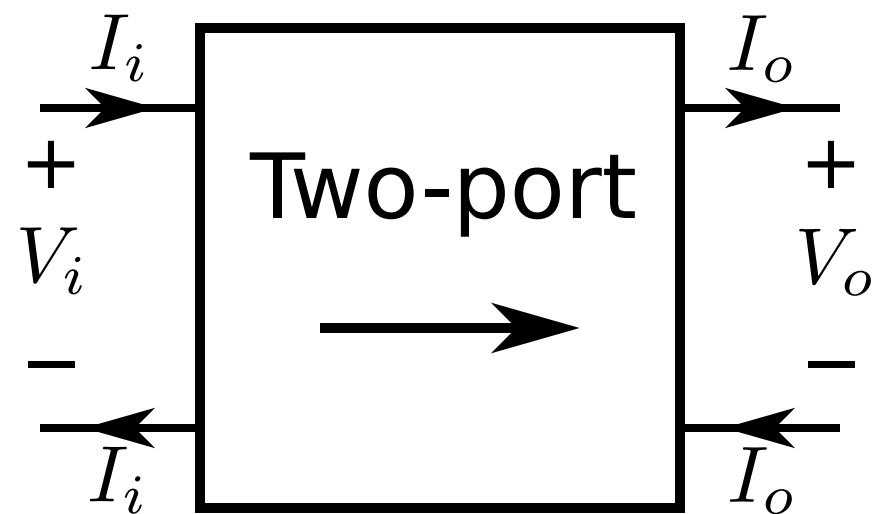


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Two-port modeling: Chapter 18.6



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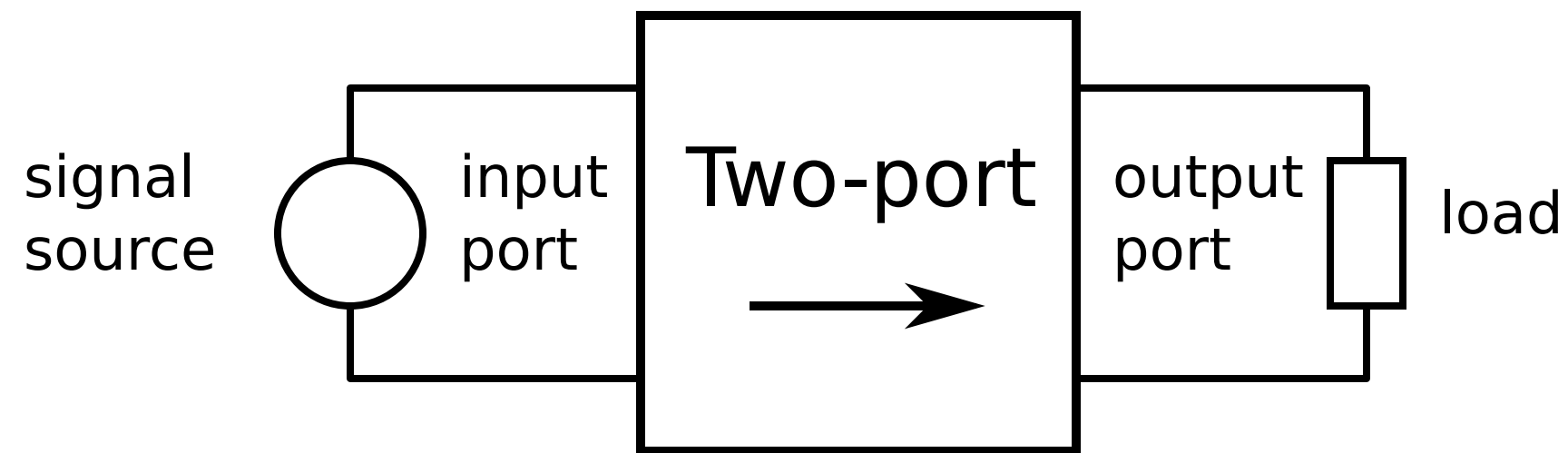
Open output

$$B = \frac{1}{\gamma} = \left. \frac{V_i}{I_o} \right|_{V_o=0},$$

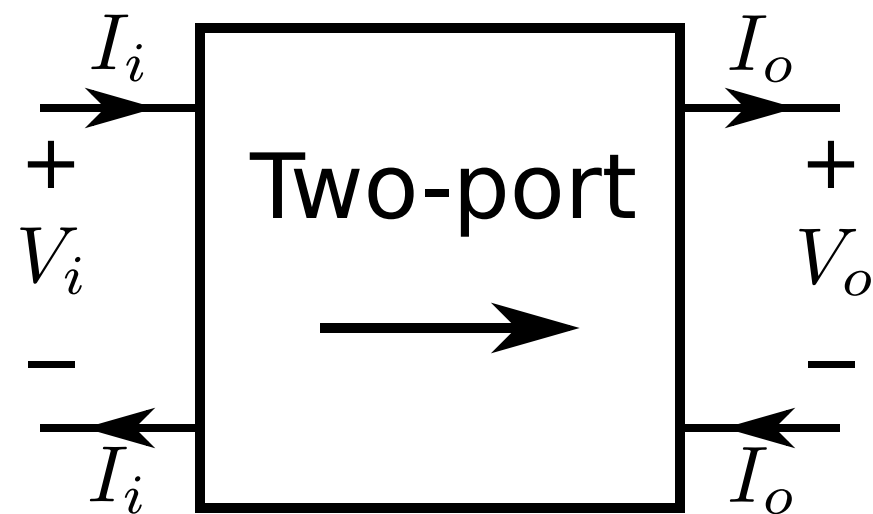
Shorted output

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Two-port modeling: Chapter 18.6



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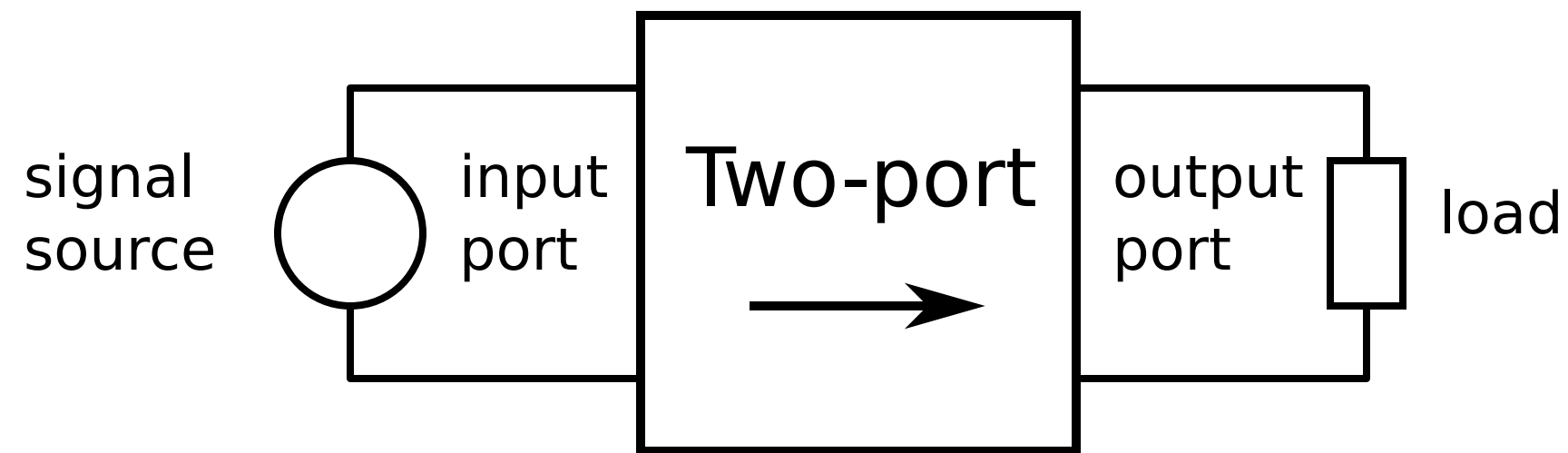
Shorted output

$$C = \frac{1}{\zeta} = \left. \frac{I_i}{V_o} \right|_{I_o=0},$$

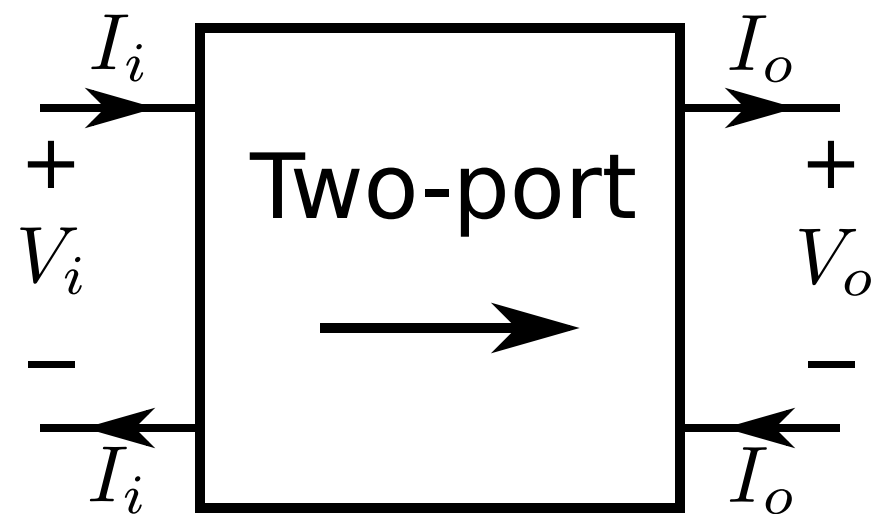
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Open output

$$B = \frac{1}{\gamma} = \left. \frac{V_i}{I_o} \right|_{V_o=0},$$

Shorted output

$$C = \frac{1}{\zeta} = \left. \frac{I_i}{V_o} \right|_{I_o=0},$$

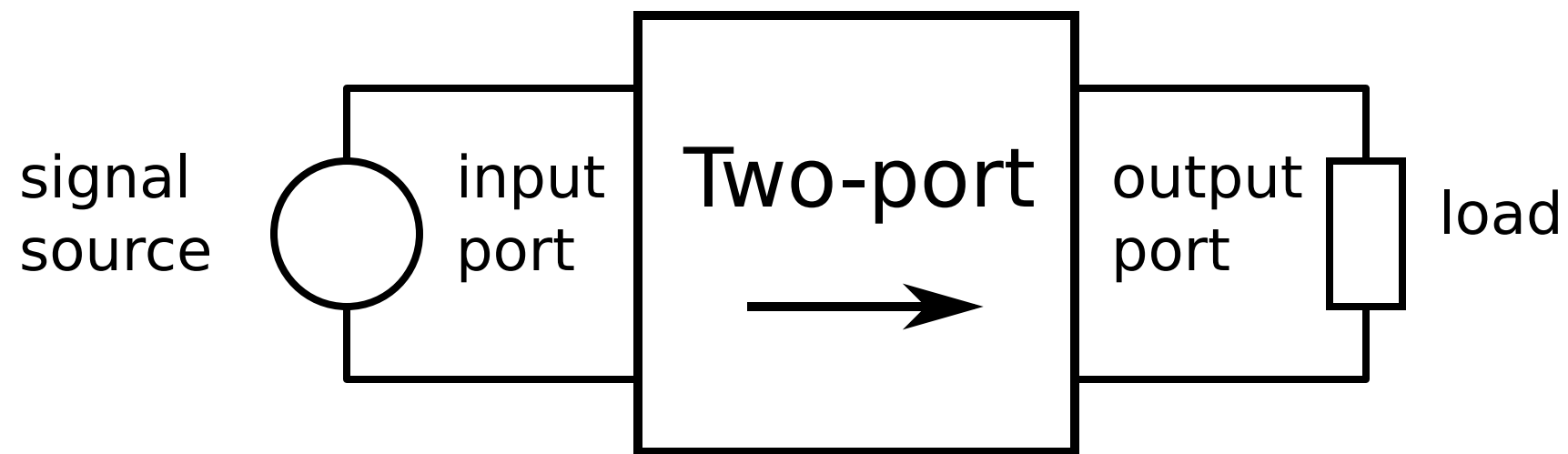
Open output

$$D = \frac{1}{\alpha} = \left. \frac{I_i}{I_o} \right|_{V_o=0}.$$

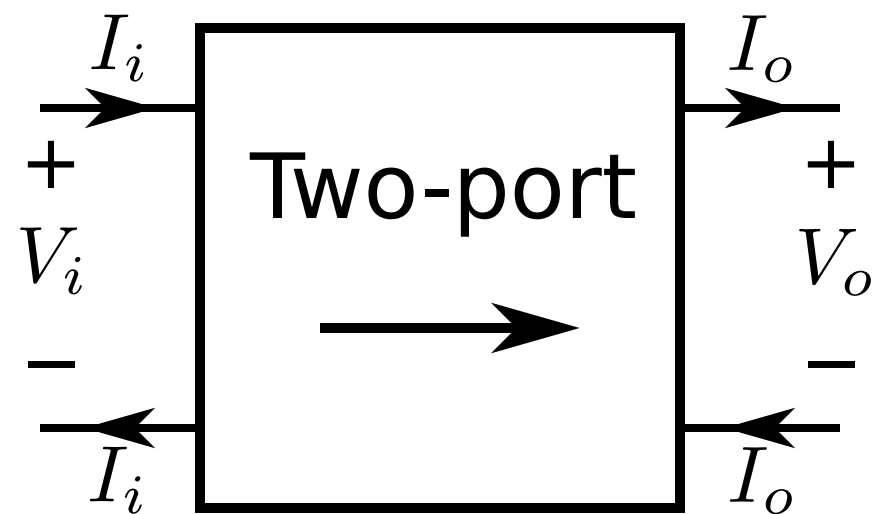
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Two-port modeling: Chapter 18.6



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$$A = \frac{1}{\mu} = \left. \frac{V_i}{V_o} \right|_{I_o=0},$$

Open output

$$B = \frac{1}{\gamma} = \left. \frac{V_i}{I_o} \right|_{V_o=0},$$

Shorted output

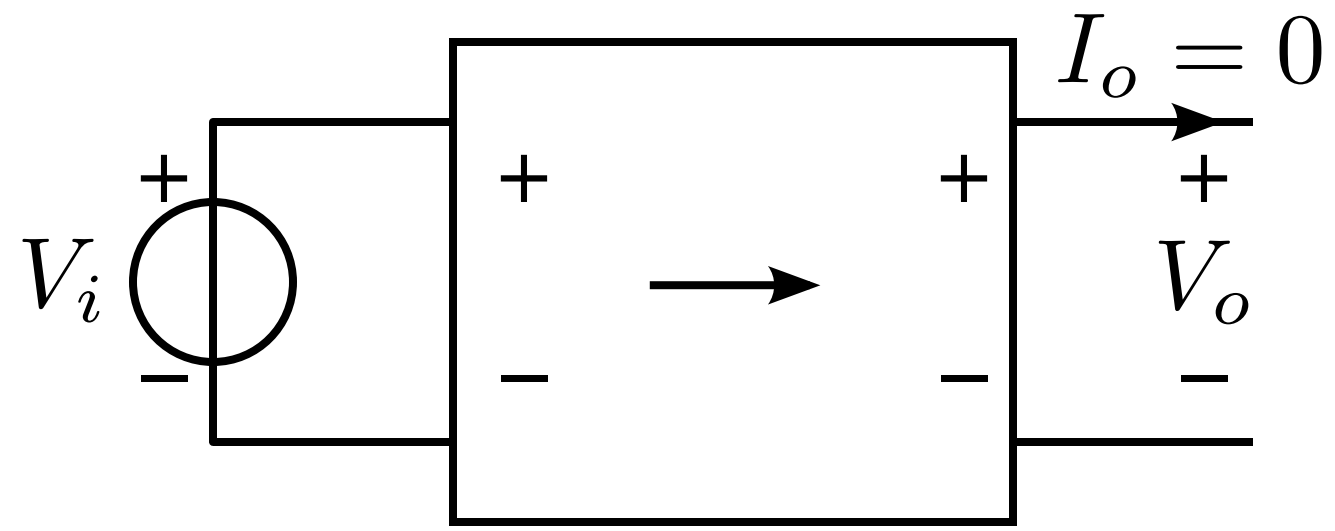
$$C = \frac{1}{\zeta} = \left. \frac{I_i}{V_o} \right|_{I_o=0},$$

Open output

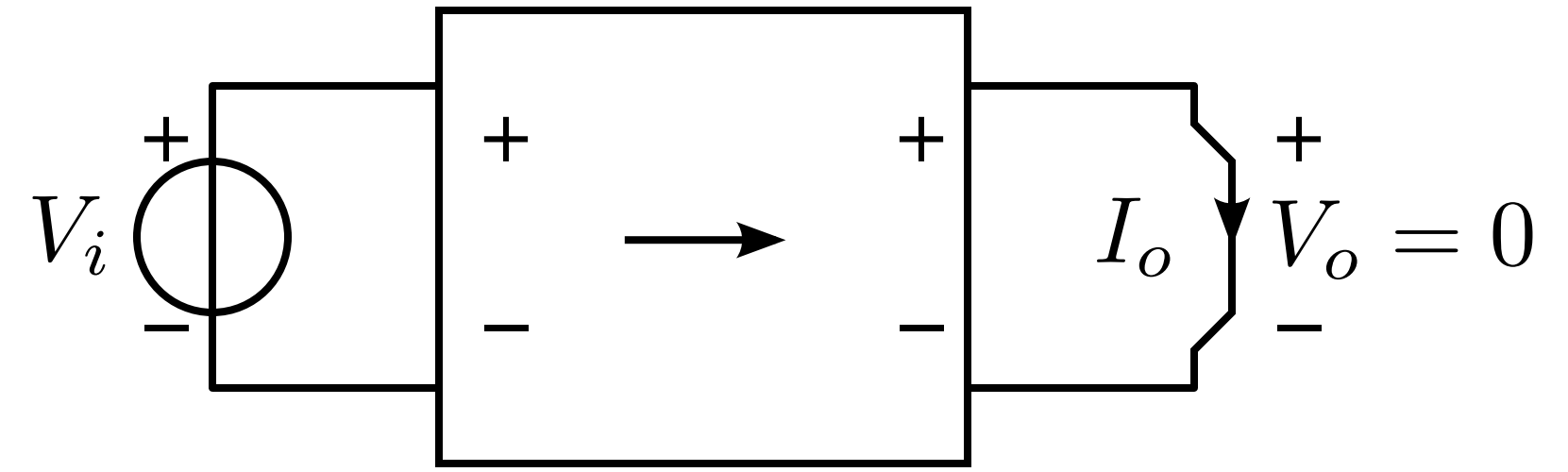
$$D = \frac{1}{\alpha} = \left. \frac{I_i}{I_o} \right|_{V_o=0}.$$

Shorted output

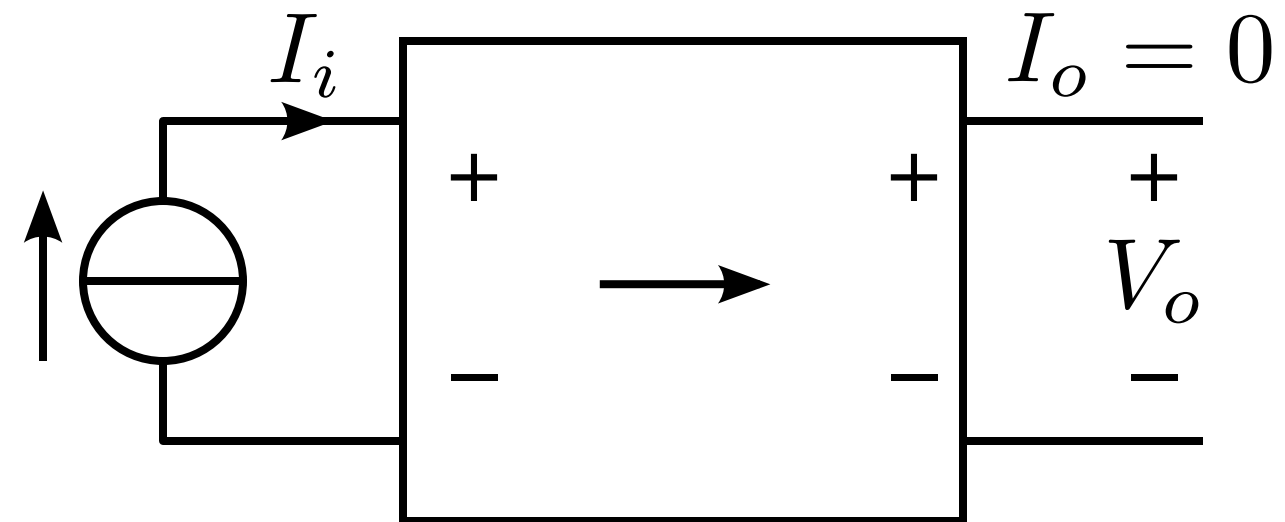
# Determination of the transmission-1 two-port parameters



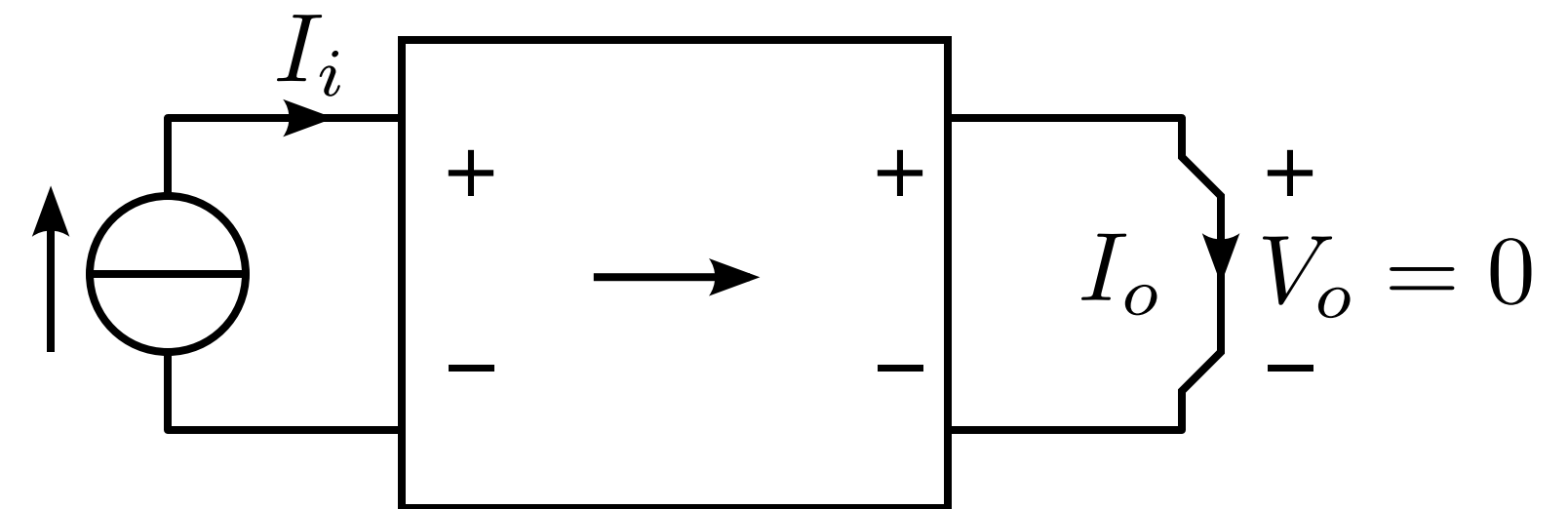
$$\mu = \frac{1}{A} = \left. \frac{V_o}{V_i} \right|_{I_o=0}$$



$$\gamma = \frac{1}{B} = \left. \frac{I_o}{V_i} \right|_{V_o=0}$$



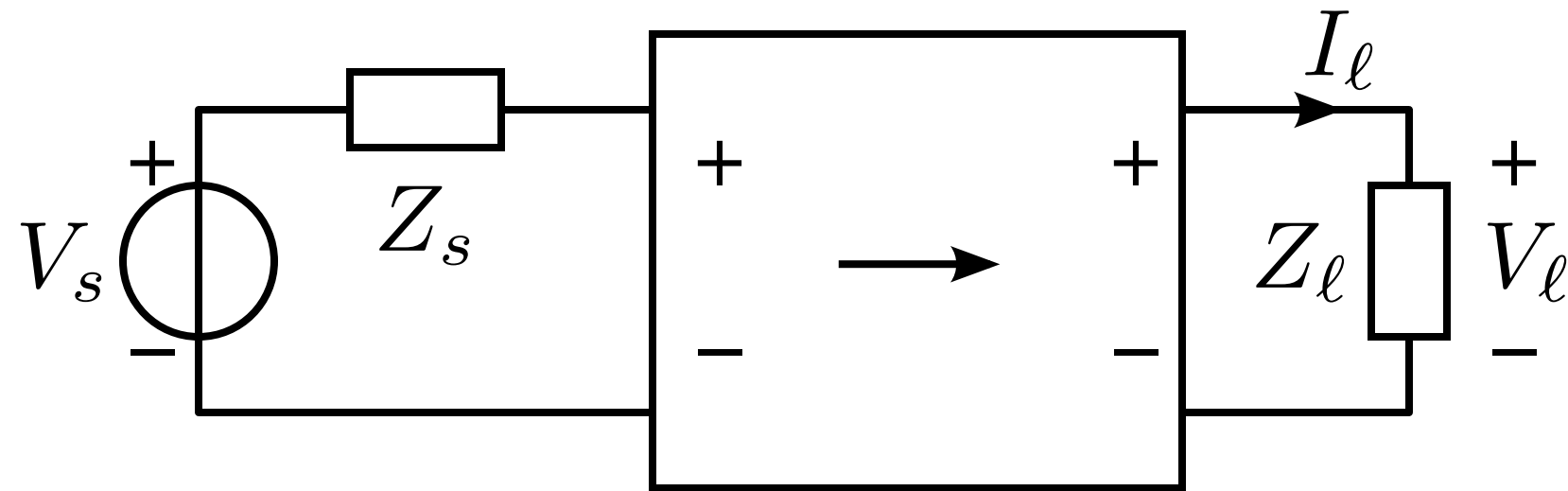
$$\zeta = \frac{1}{C} = \left. \frac{V_o}{I_i} \right|_{I_o=0}$$



$$\alpha = \frac{1}{D} = \left. \frac{I_o}{I_i} \right|_{V_o=0}$$

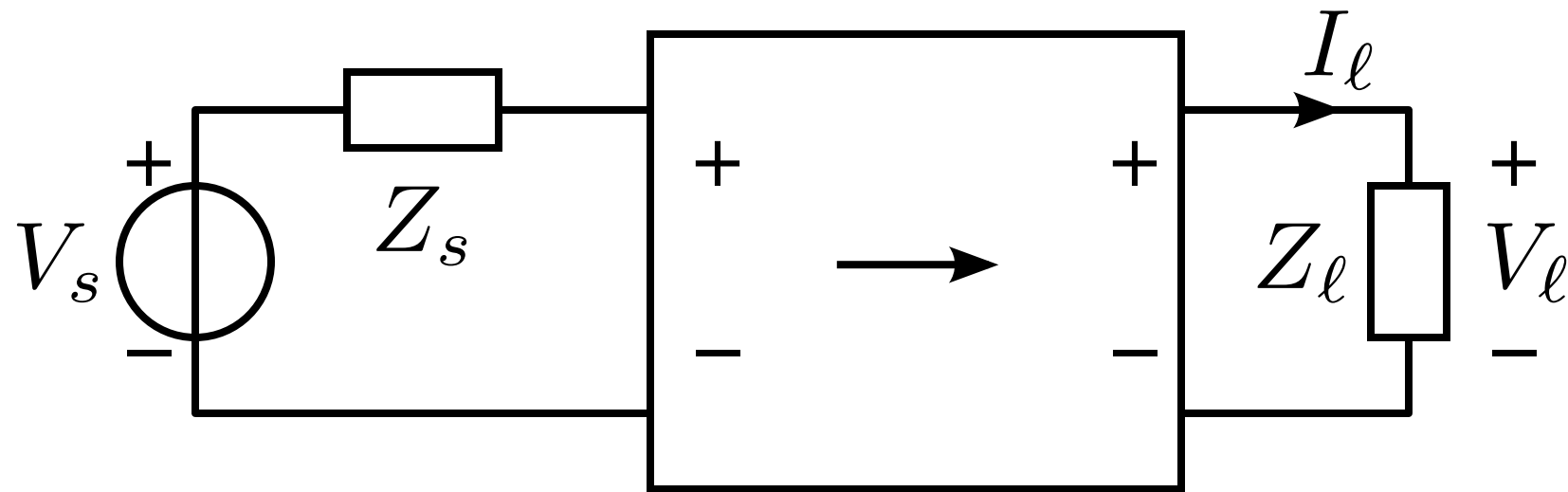
# Source to load transfer

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$$A_v = \frac{V_\ell}{V_s} = \frac{1}{A + B \frac{1}{Z_\ell} + C Z_s + D \frac{Z_s}{Z_\ell}}$$

# Source to load transfer

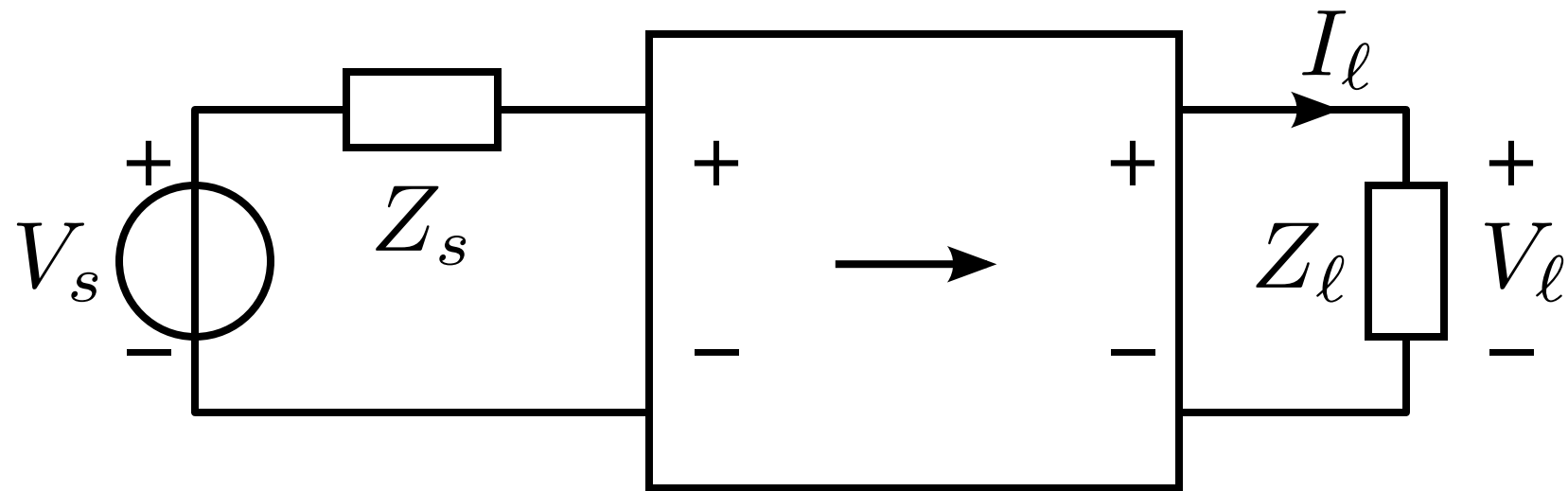


$$A_v = \frac{V_\ell}{V_s} = \frac{1}{\textcolor{blue}{A} + B \frac{1}{Z_\ell} + C Z_s + D \frac{Z_s}{Z_\ell}}$$

$$A_y = \frac{I_\ell}{V_s} = \frac{1}{A Z_\ell + \textcolor{blue}{B} + C Z_\ell Z_s + D Z_s}$$

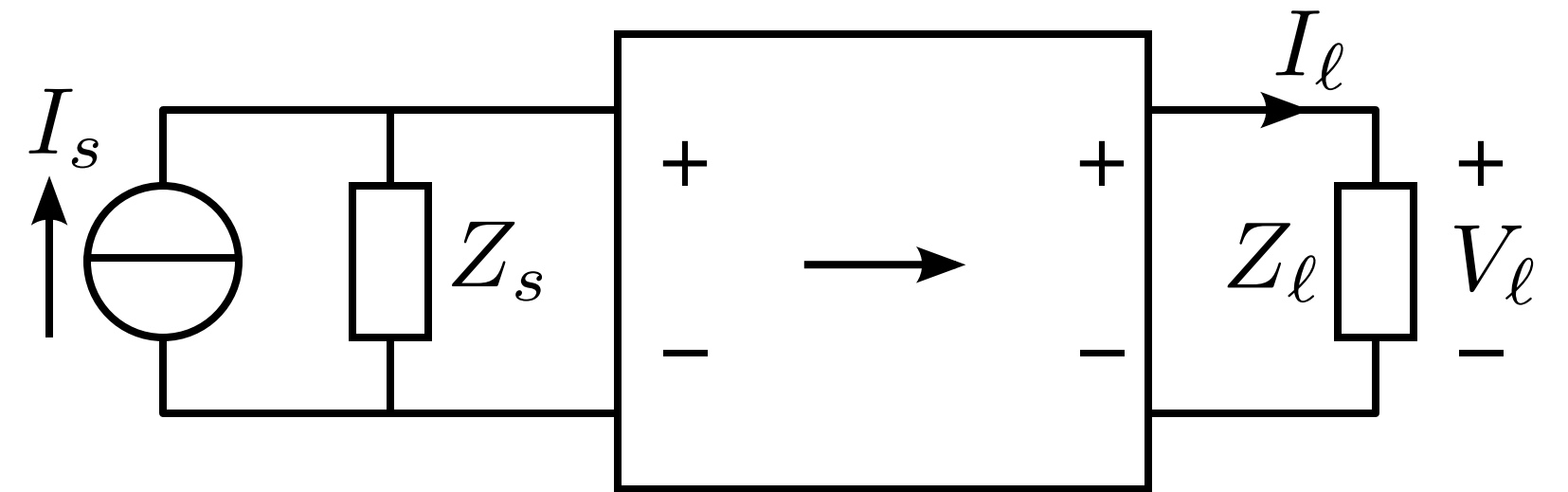


# Source to load transfer



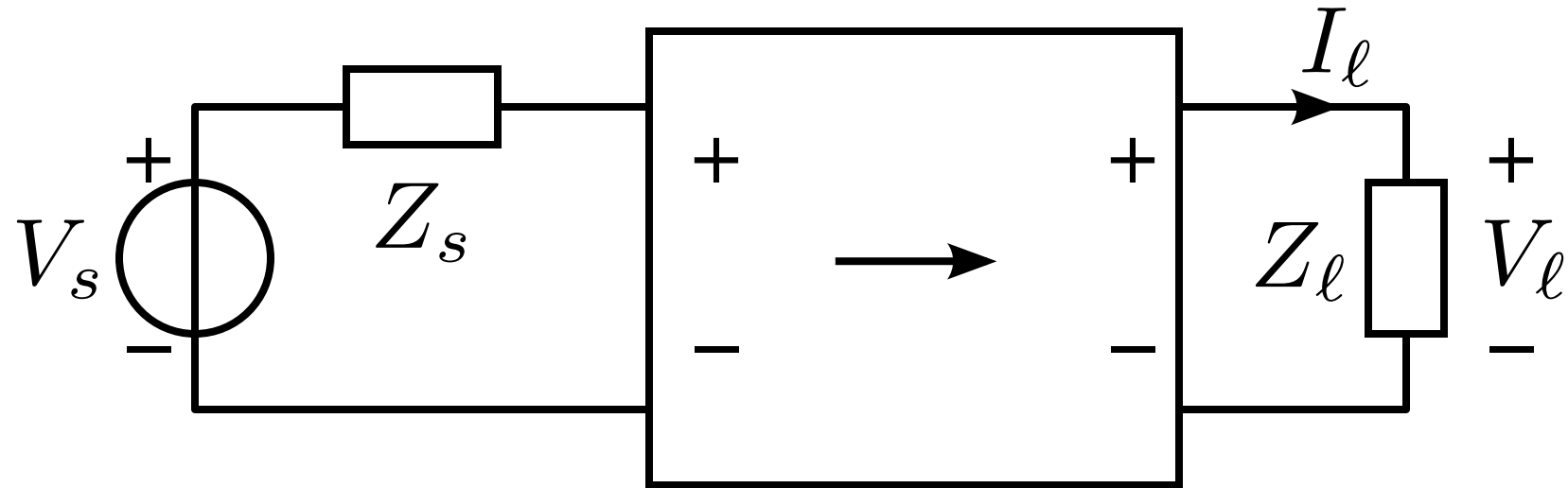
$$A_v = \frac{V_\ell}{V_s} = \frac{1}{A + B \frac{1}{Z_\ell} + C Z_s + D \frac{Z_s}{Z_\ell}}$$

$$A_y = \frac{I_\ell}{V_s} = \frac{1}{A Z_\ell + B + C Z_\ell Z_s + D Z_s}$$



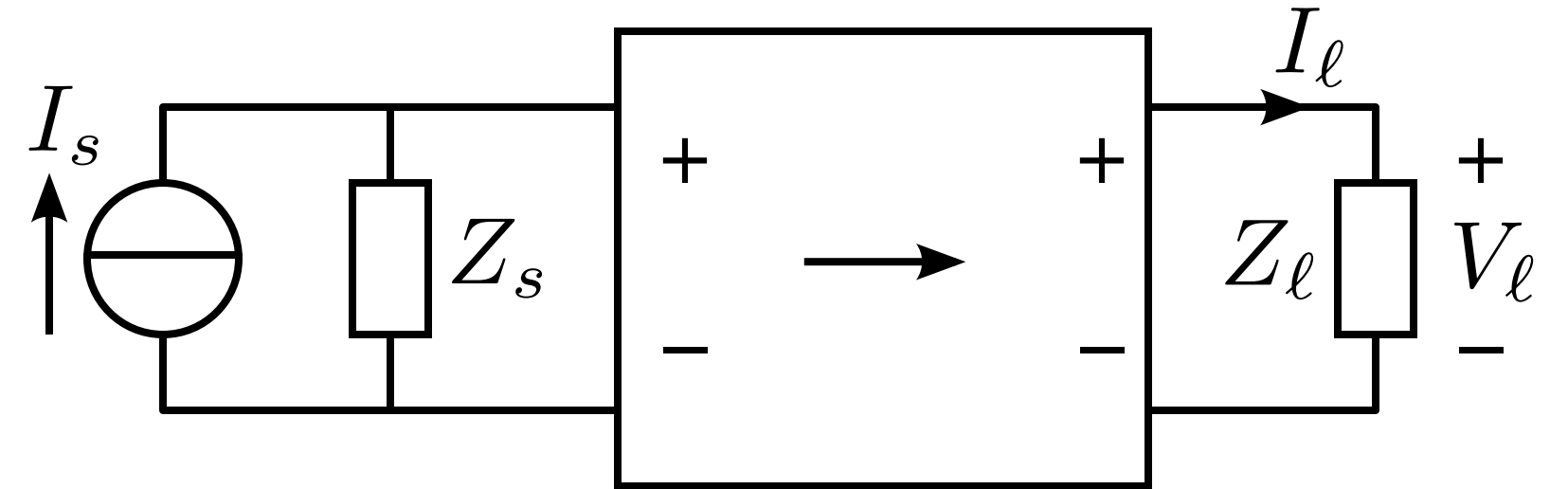
$$A_z = \frac{V_\ell}{I_s} = \frac{1}{A \frac{1}{Z_s} + B \frac{1}{Z_s Z_\ell} + C + D \frac{1}{Z_\ell}}$$

# Source to load transfer



$$A_v = \frac{V_\ell}{V_s} = \frac{1}{A + B \frac{1}{Z_\ell} + C Z_s + D \frac{Z_s}{Z_\ell}}$$

$$A_y = \frac{I_\ell}{V_s} = \frac{1}{A Z_\ell + B + C Z_\ell Z_s + D Z_s}$$

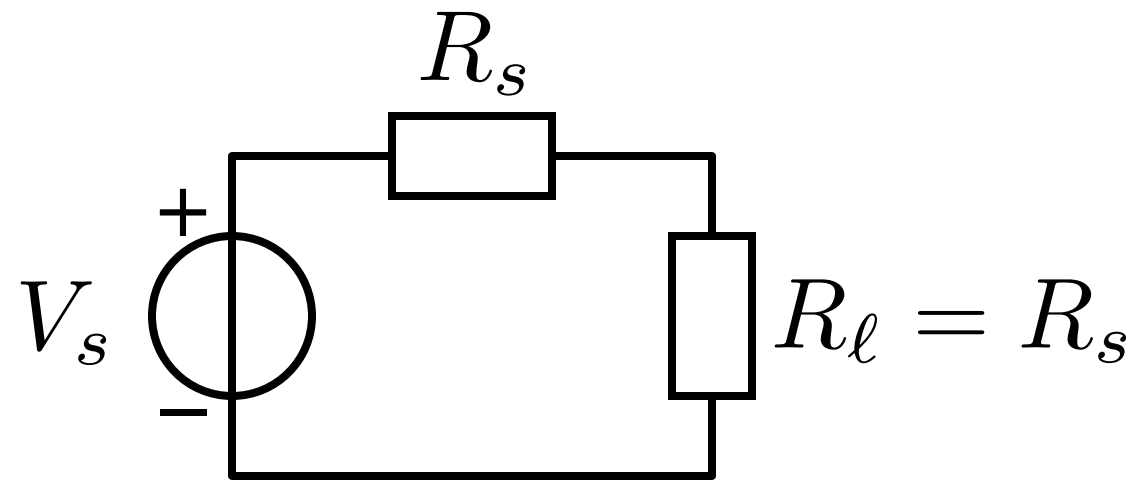


$$A_z = \frac{V_\ell}{I_s} = \frac{1}{A \frac{1}{Z_s} + B \frac{1}{Z_s Z_\ell} + C + D \frac{1}{Z_\ell}}$$

$$A_i = \frac{I_\ell}{I_s} = \frac{1}{A \frac{Z_\ell}{Z_s} + B \frac{1}{Z_s} + C Z_\ell + D}$$

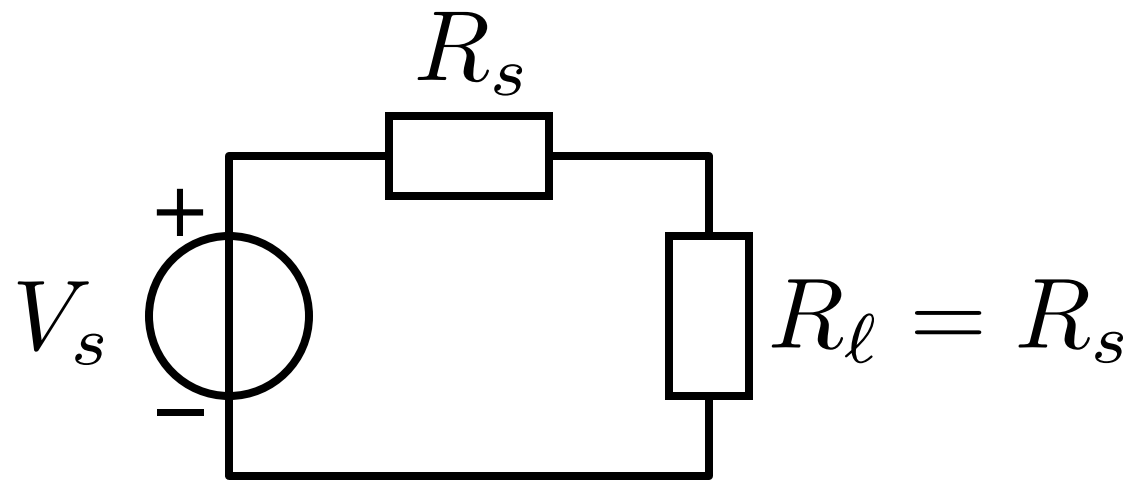
# Available power gain

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Available power of the source

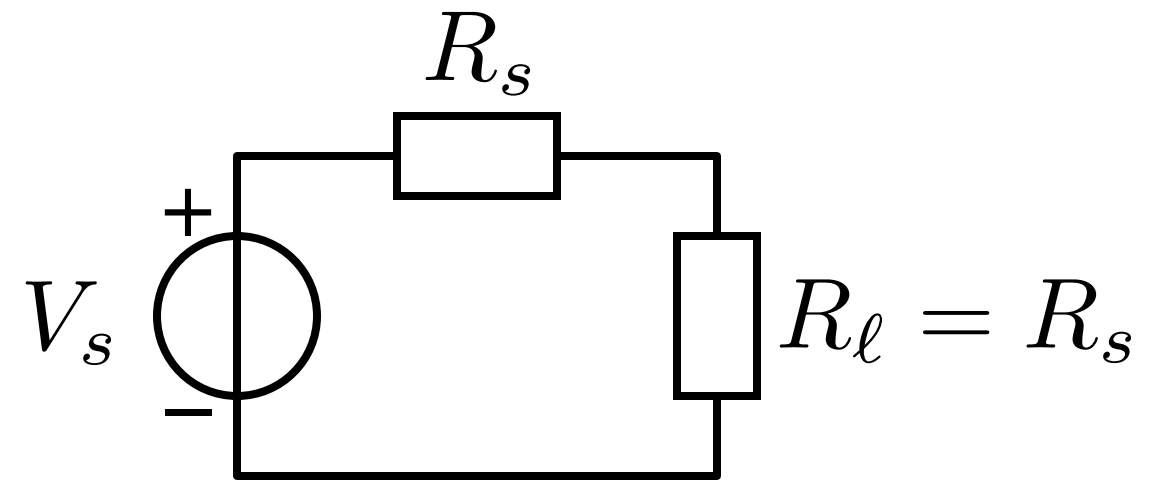
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Available power of the source

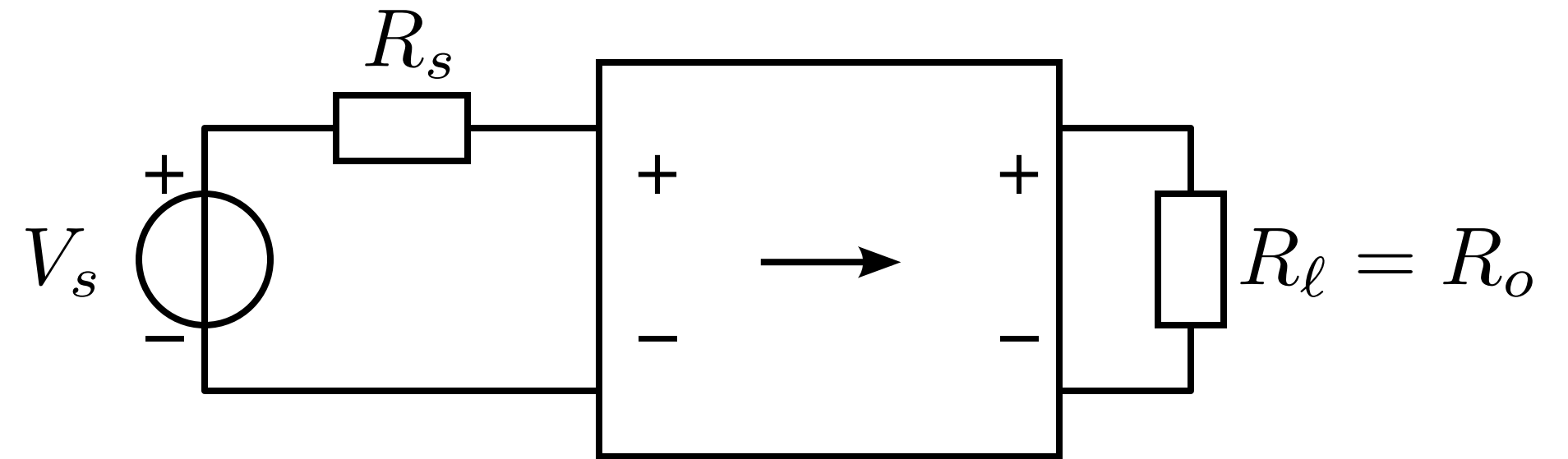
$$P_s = \frac{V_s^2}{4R_s}$$

# Available power gain



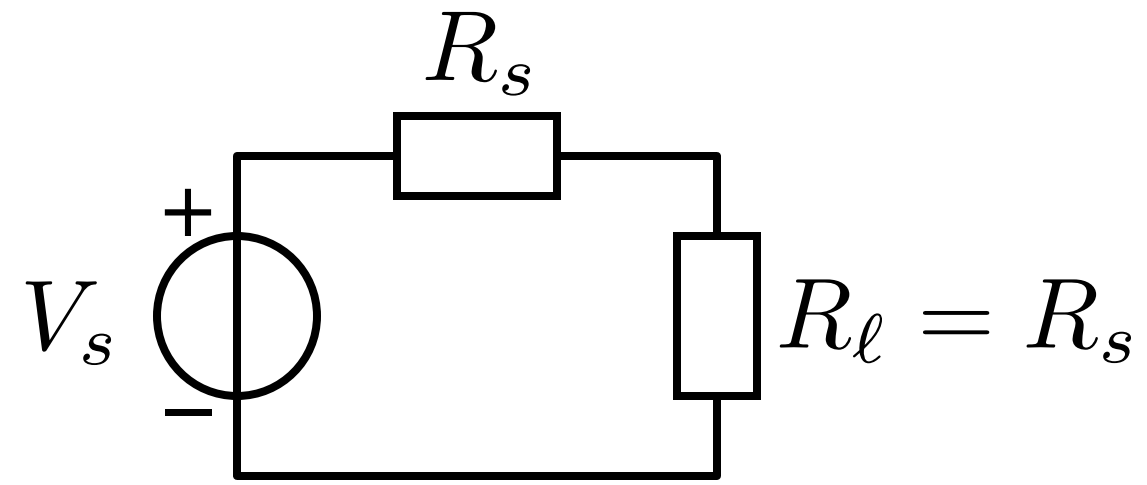
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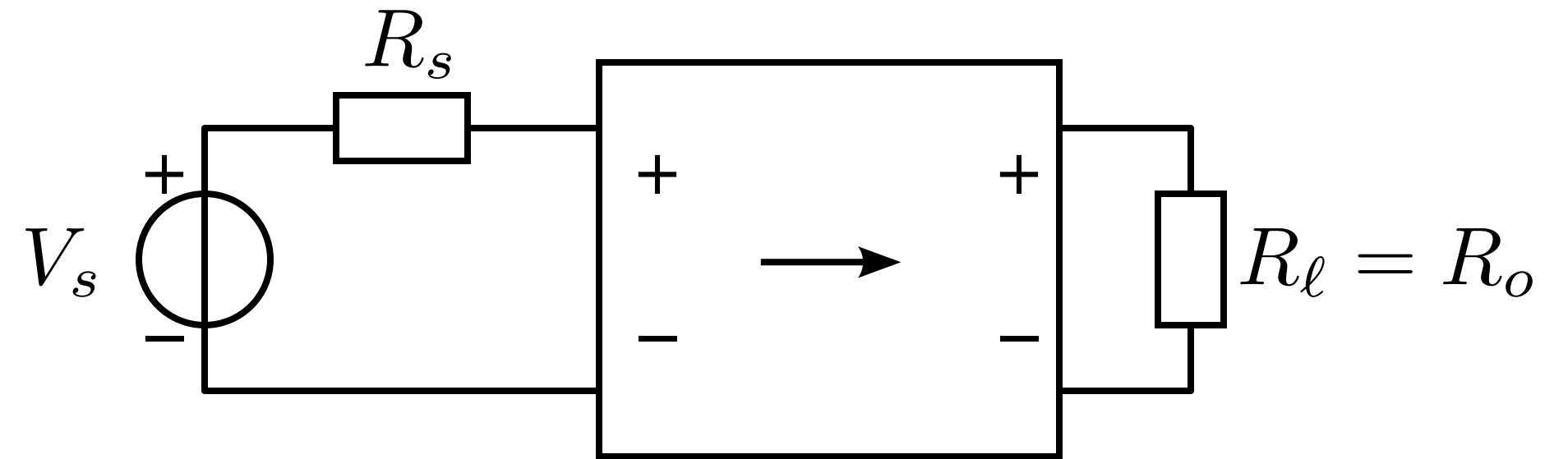
Available power of the amplifier  
connected to the source

# Available power gain



Available power of the source

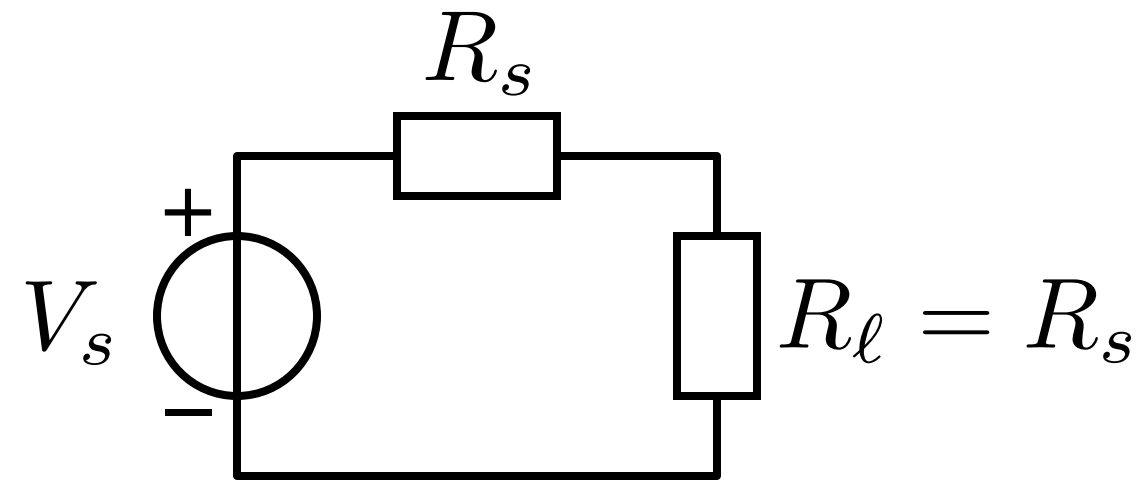
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Available power of the amplifier  
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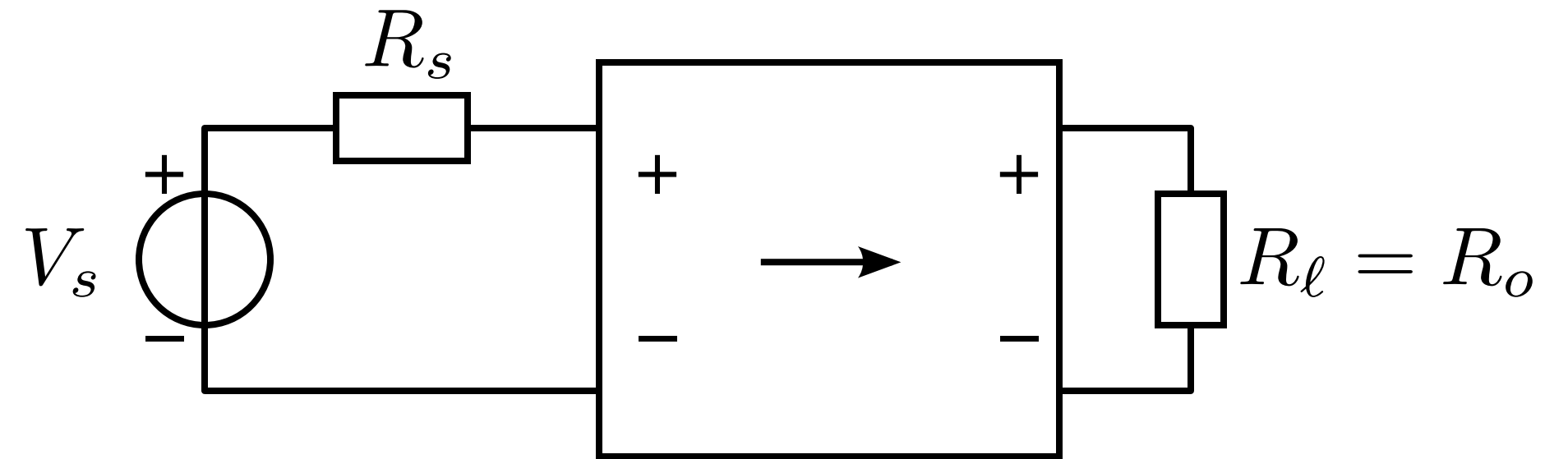
$$P_a = \frac{V_s^2}{4(DR_s + B)(CR_s + A)}$$

## Available power gain



Available power of the source

$$P_s = \frac{V_s^2}{4R_s}$$



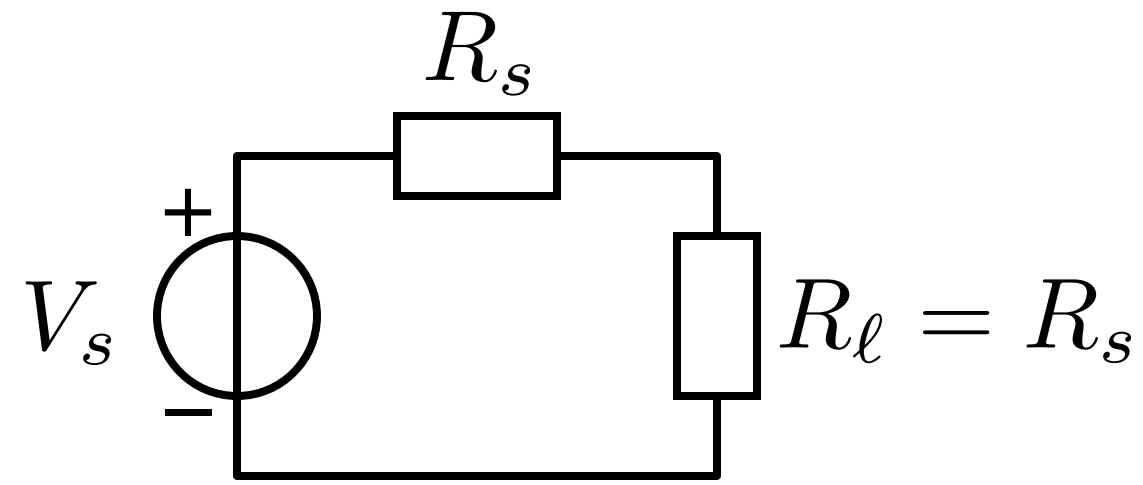
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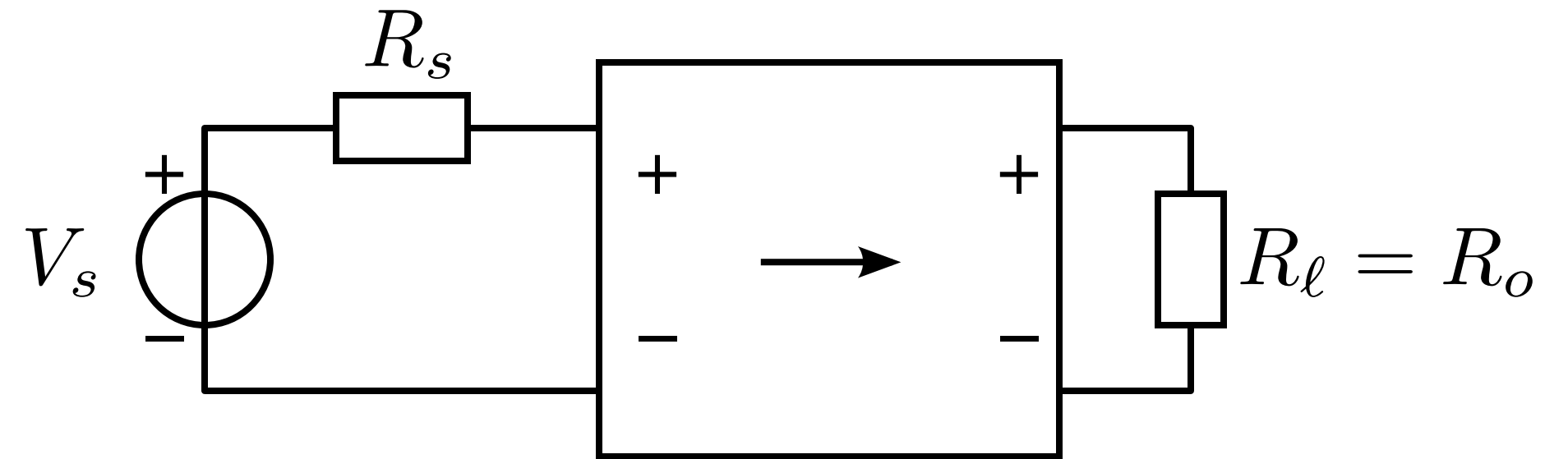


# Available power gain



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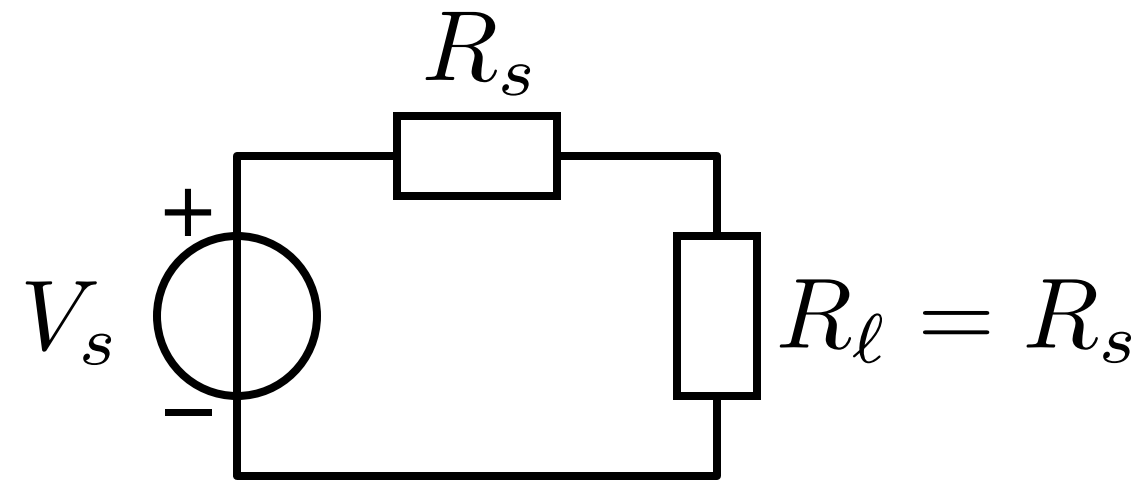
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Available power gain

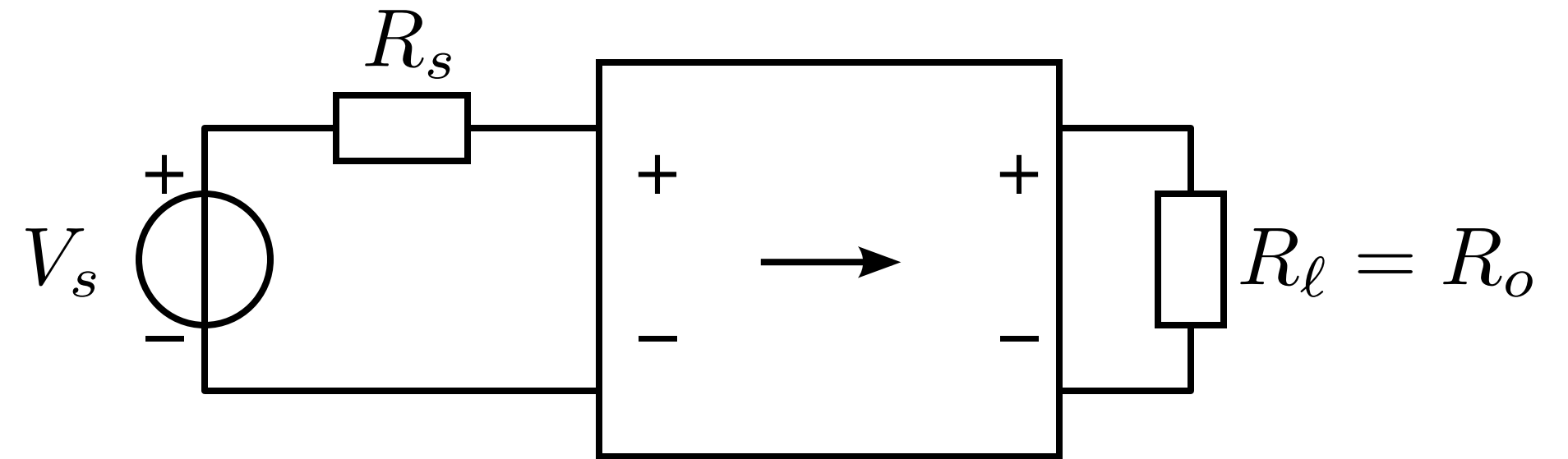
$$G_p = \frac{P_a}{P_s} = \frac{1}{AD + AB/R_s + BC + CDR_s}$$

# Available power gain



Available power of the source

$$P_s = \frac{V_s^2}{4R_s}$$



Available power of the amplifier  
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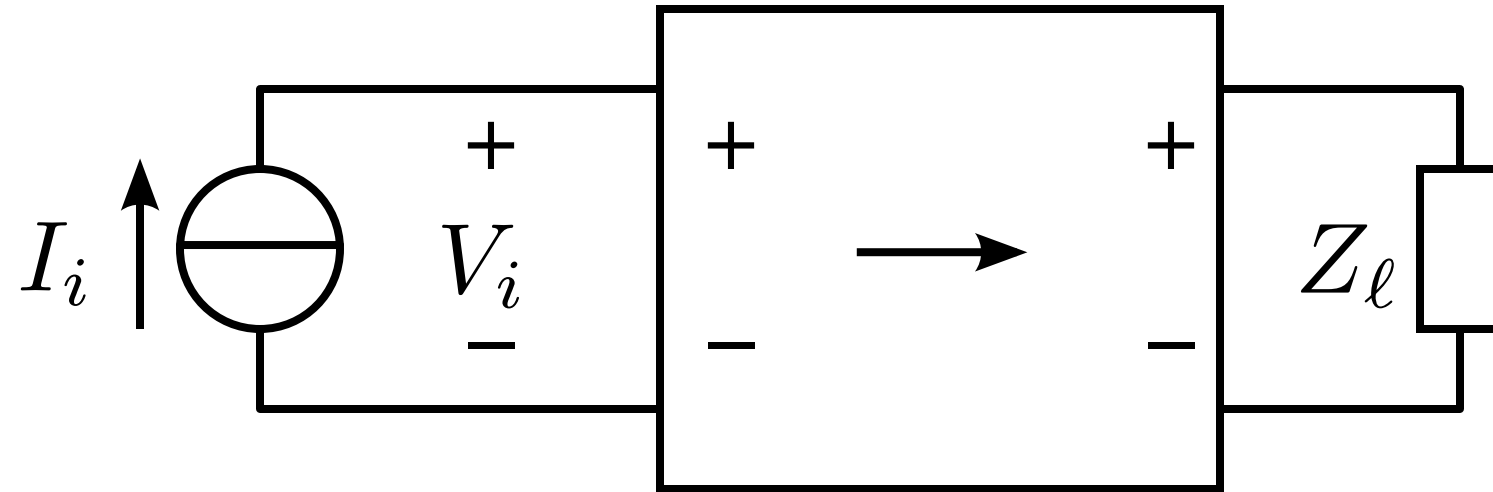
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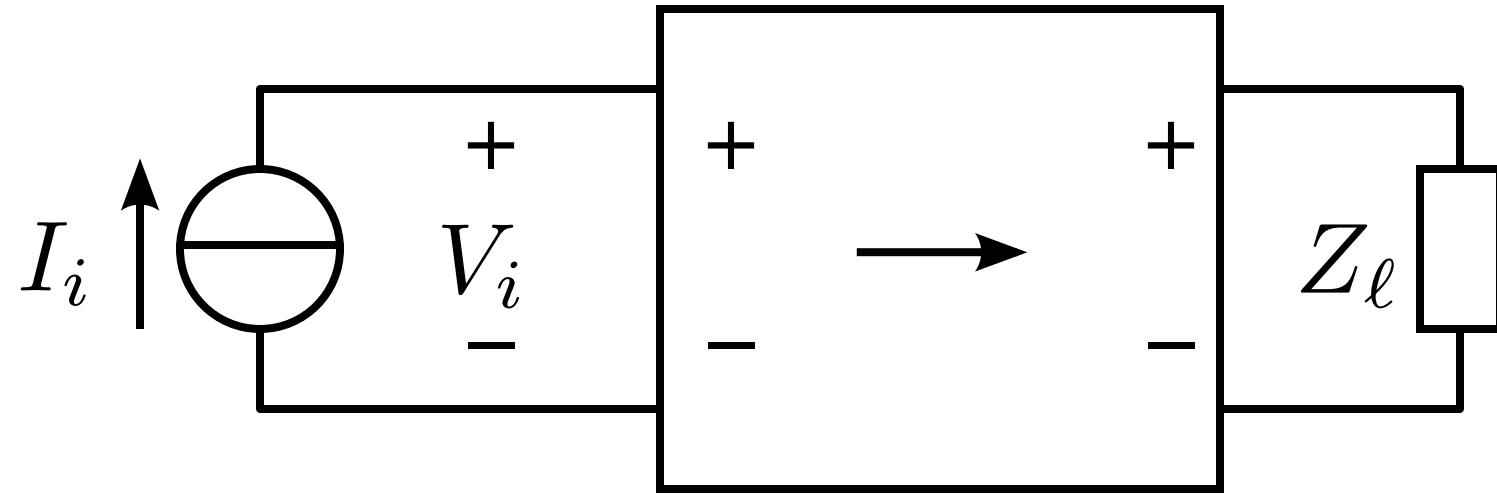
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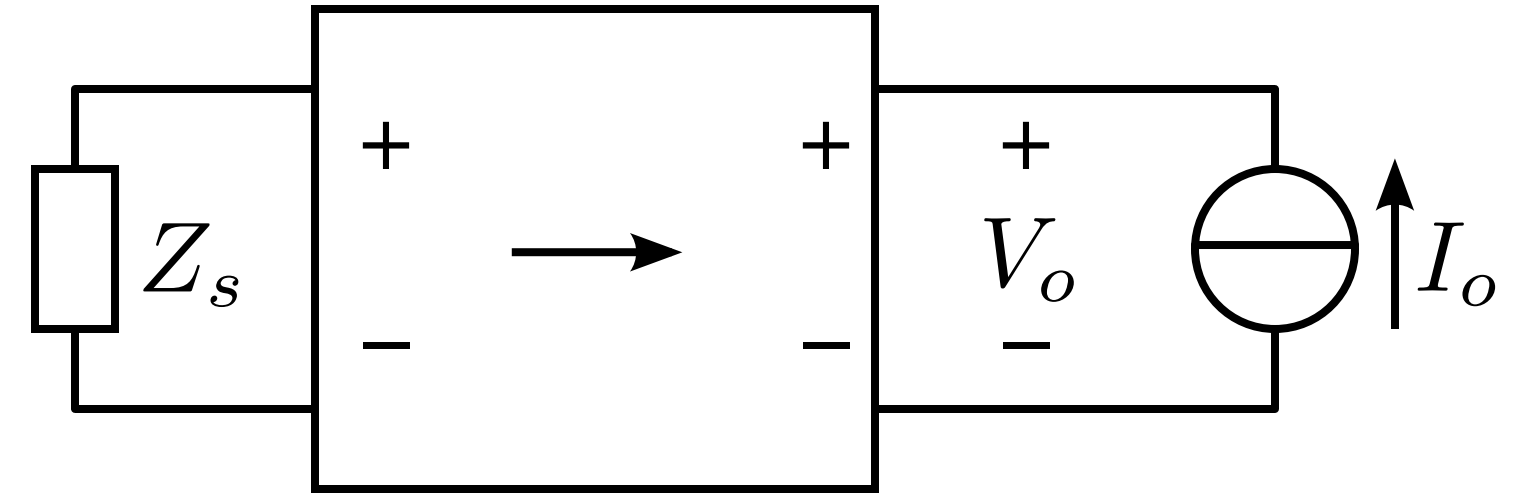


$$Z_i = \frac{V_i}{I_i} = \frac{AZ_\ell + B}{CZ_\ell + D}$$

# Port impedances

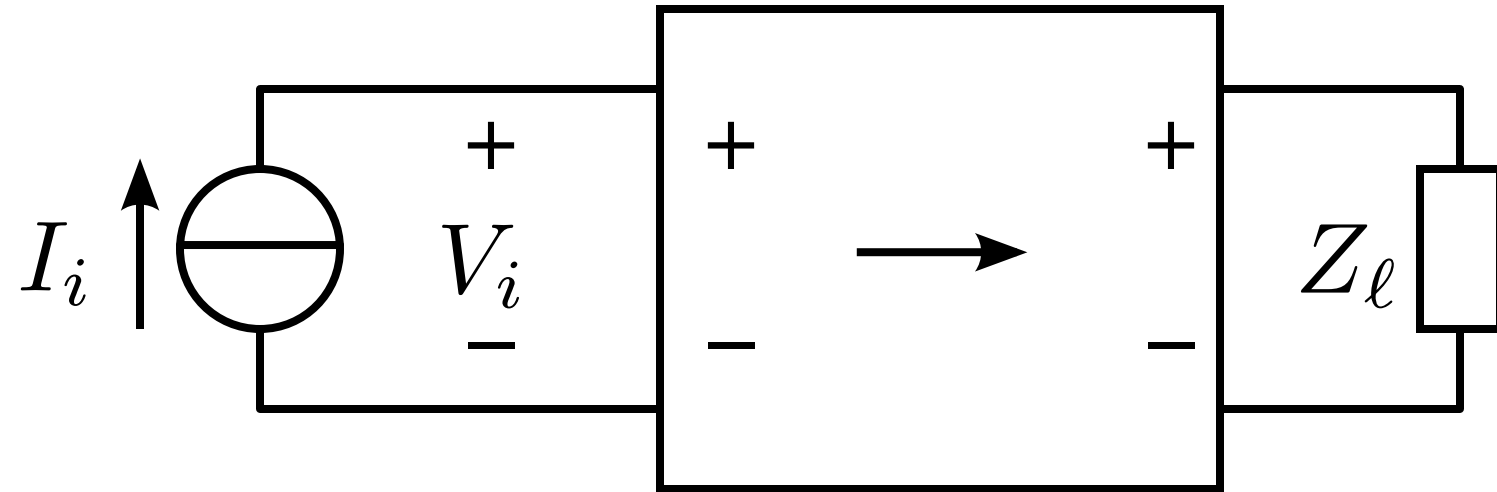


$$Z_i = \frac{V_i}{I_i} = \frac{AZ_\ell + B}{CZ_\ell + D}$$

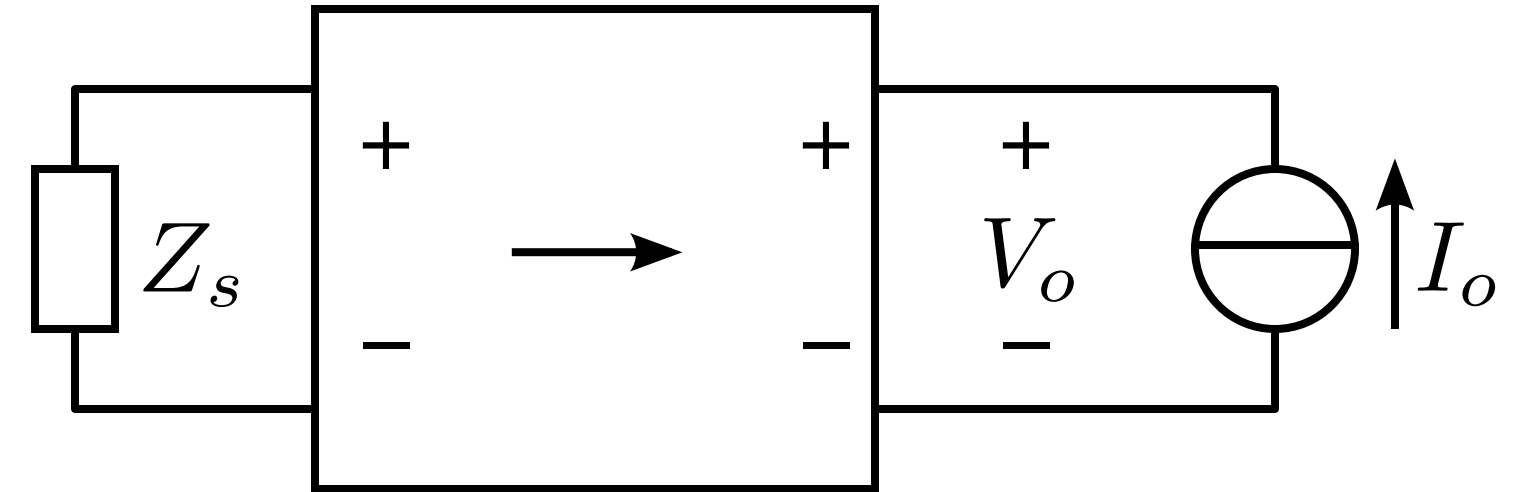


$$Z_o = \frac{V_o}{I_o} = \frac{DZ_s + B}{CZ_s + A}$$

# Port impedances



$$Z_i = \frac{V_i}{I_i} = \frac{AZ_\ell + B}{CZ_\ell + D}$$

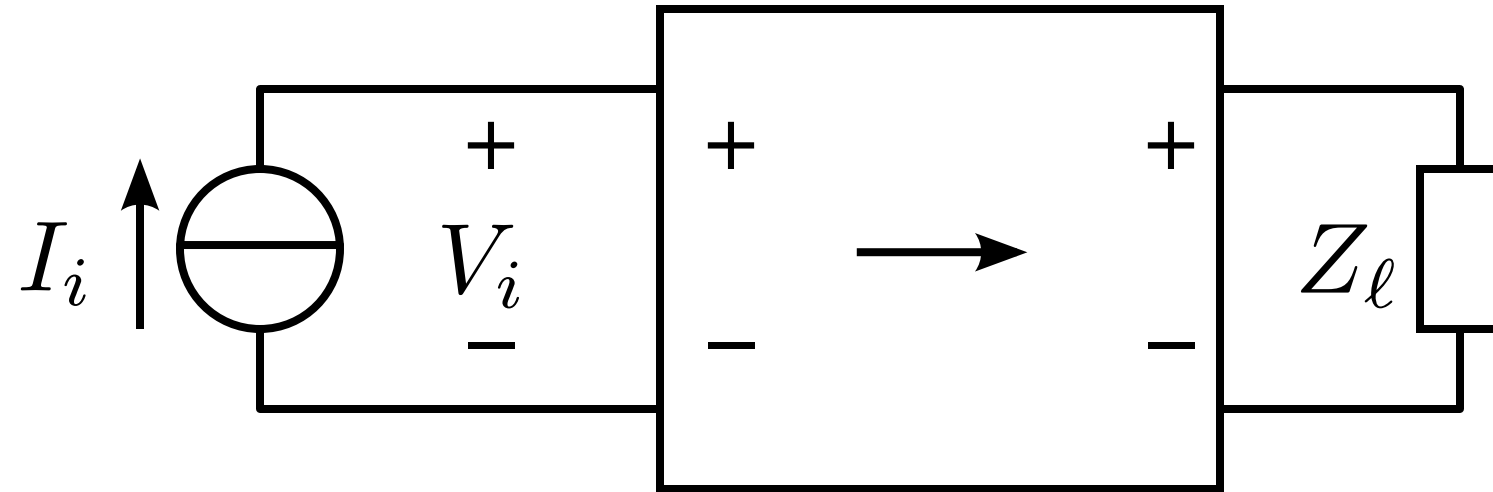


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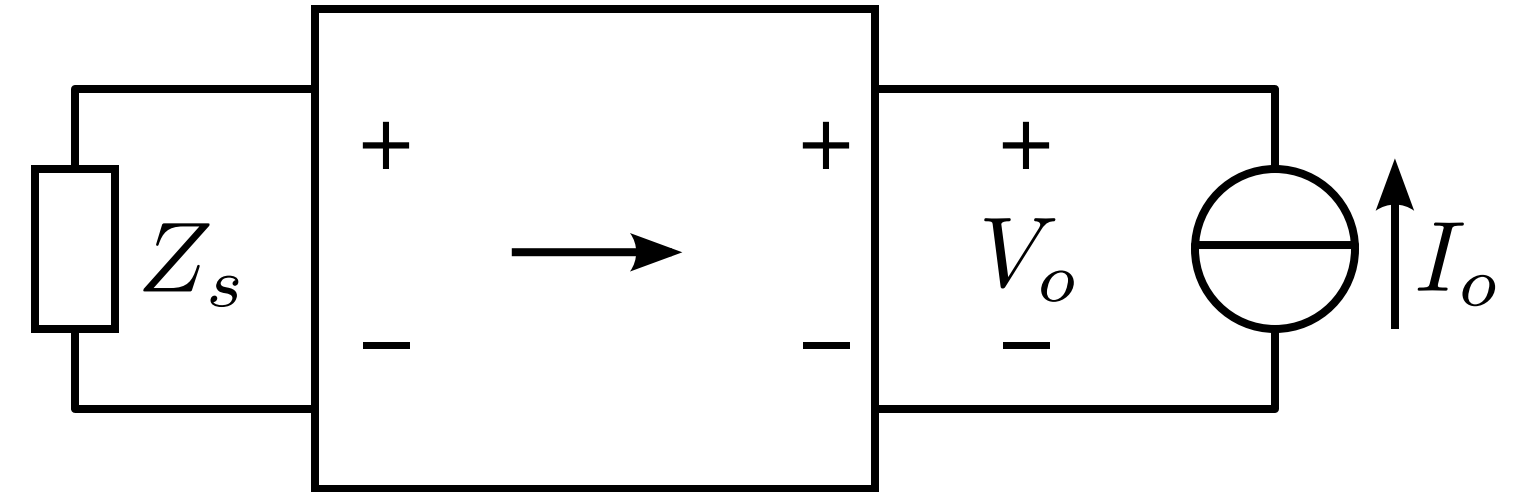
Unilateral if:

$$AD = BC$$

# Port impedances



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Unilateral if:

$$AD = BC$$

# Amplifier types

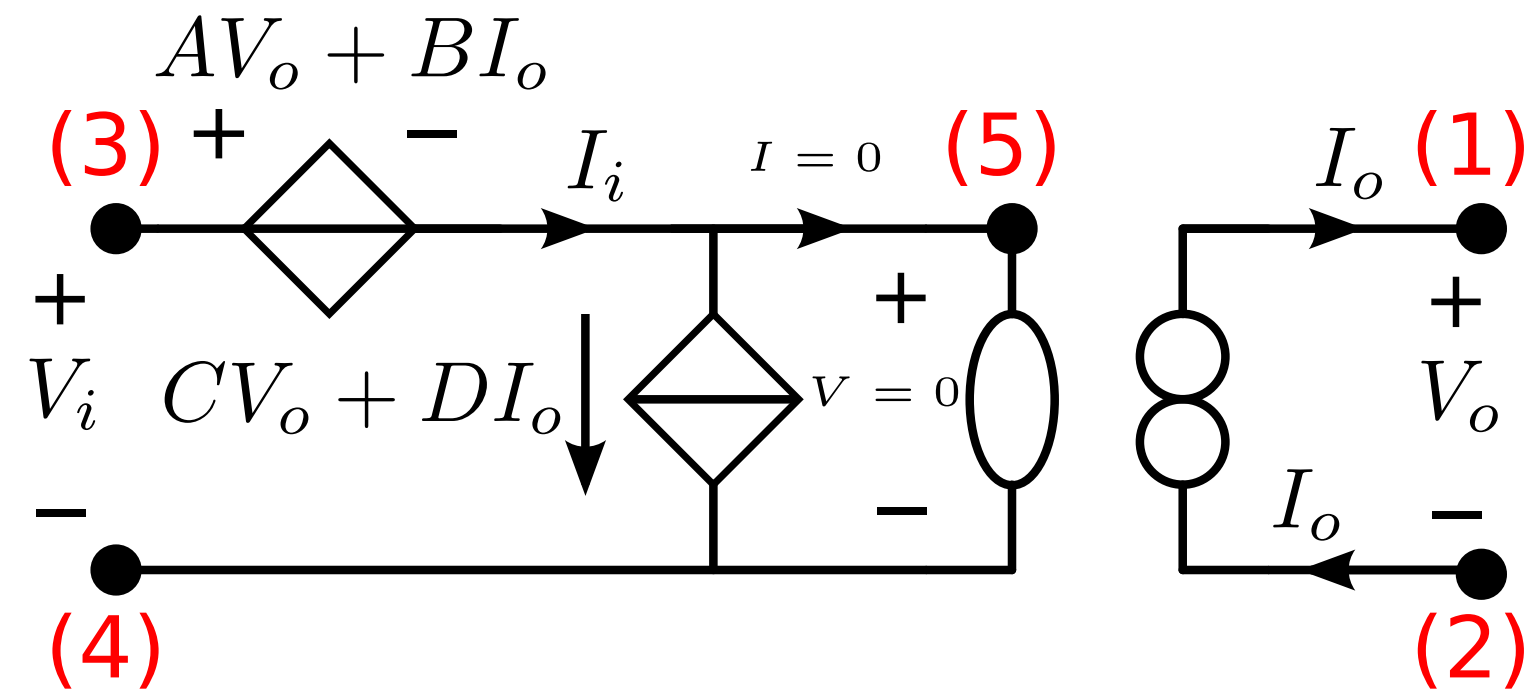


# Amplifier types

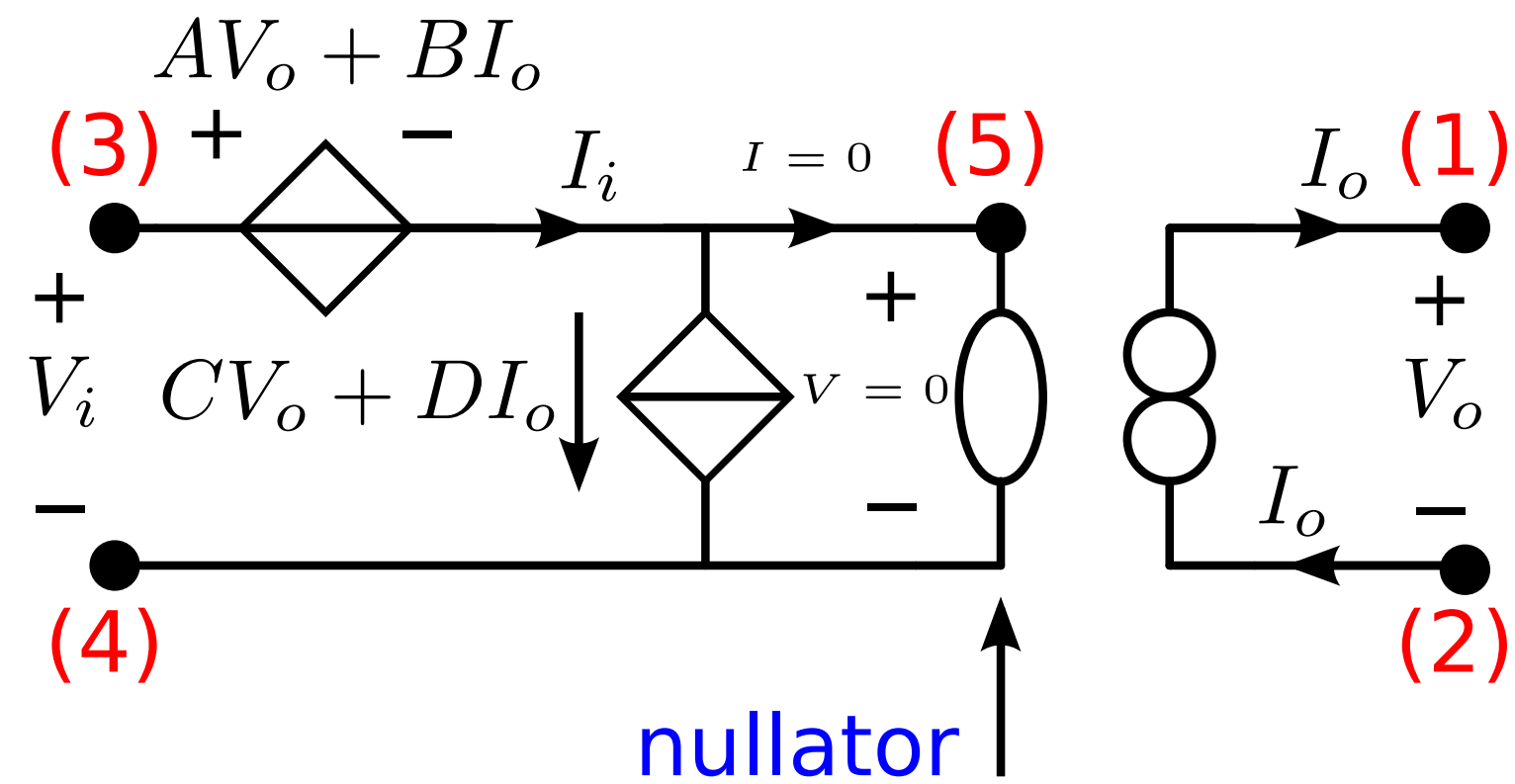
no	amplifier type	$Z_i$	$Z_o$	$A$	$B$	$C$	$D$
1	Voltage amplifier	$\infty$	0	$A$	0	0	0
2	Transadmittance amplifier	$\infty$	$\infty$	0	$B$	0	0
3	Voltage input, finite nonzero output impedance	$\infty$	$Z_o$	$A$	$B$	0	0
4	Transimpedance amplifier	0	0	0	0	$C$	0
5	Current amplifier	0	$\infty$	0	0	0	$D$
6	Current input, finite nonzero output impedance	0	$Z_o$	0	0	$C$	$D$
7	Finite nonzero input impedance, voltage output	$Z_i$	0	$A$	0	$C$	0
8	Finite nonzero input impedance, current output	$Z_i$	$\infty$	0	$B$	0	$D$
9	Finite nonzero input and output impedance	$Z_i$	$Z_o$	$A$	$B$	$C$	$D$

# Generalized two-port model

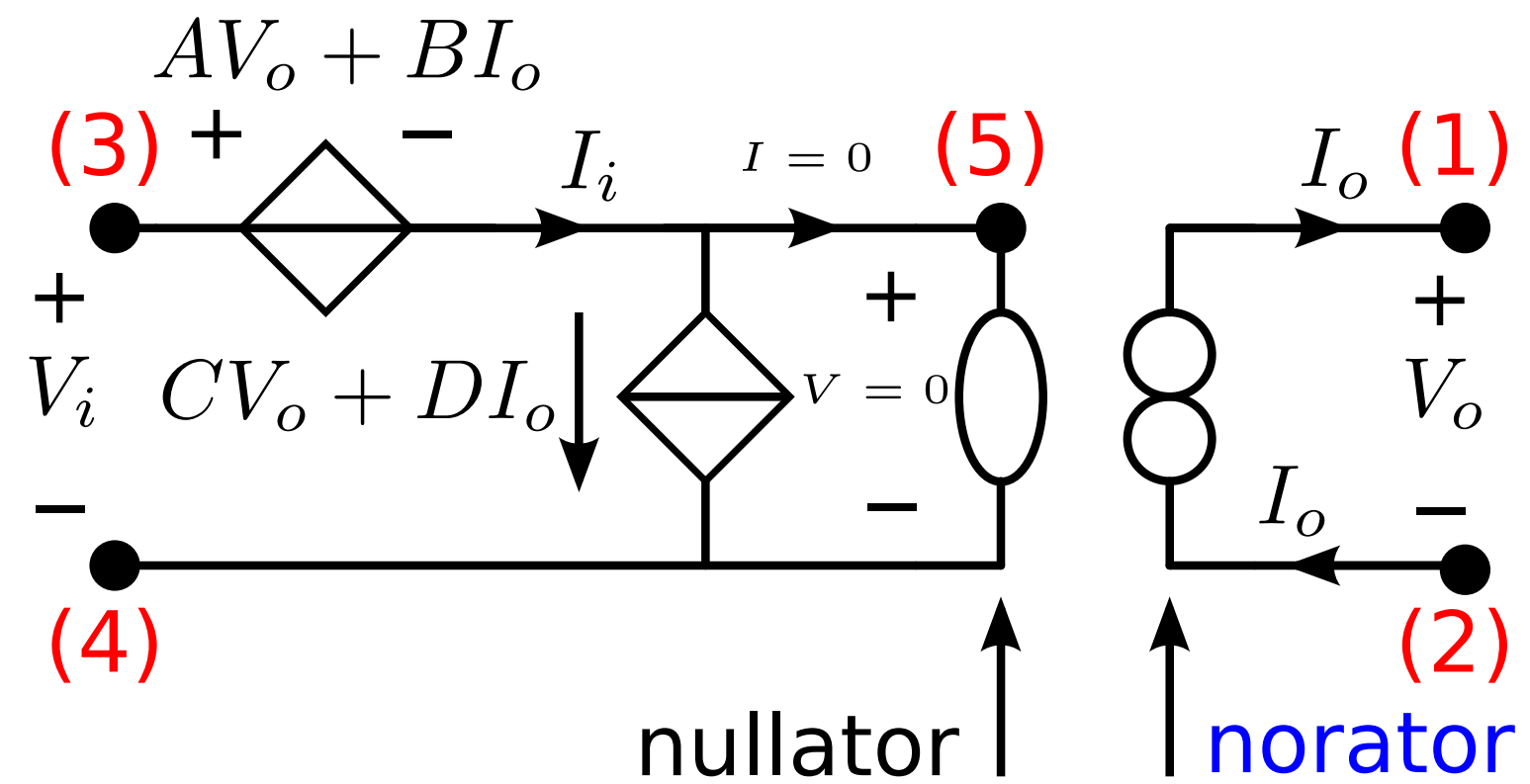
# Generalized two-port model



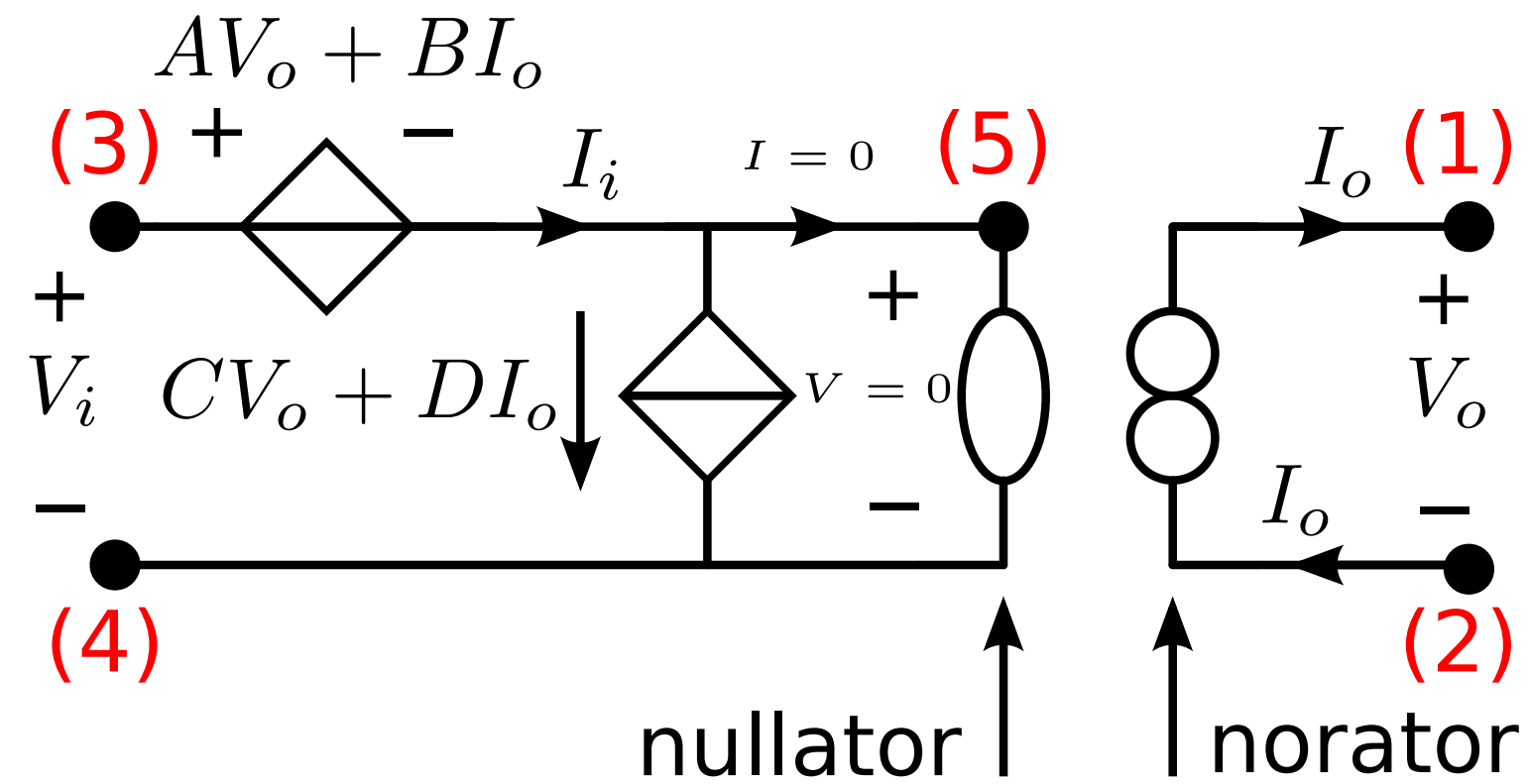
# Generalized two-port model



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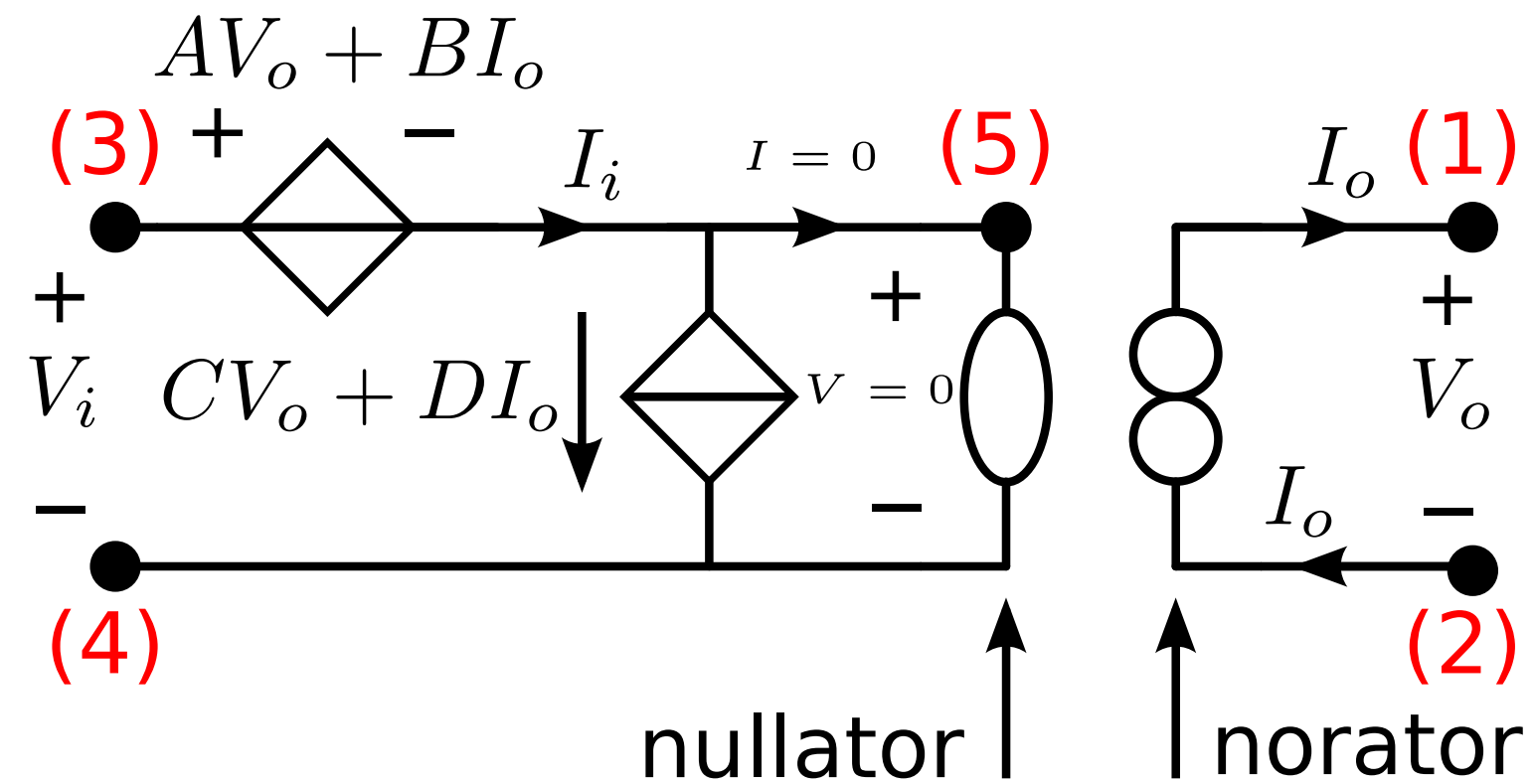


# Generalized two-port model



Nullator and norator always  
in pairs in a network  
See section 18.3.3

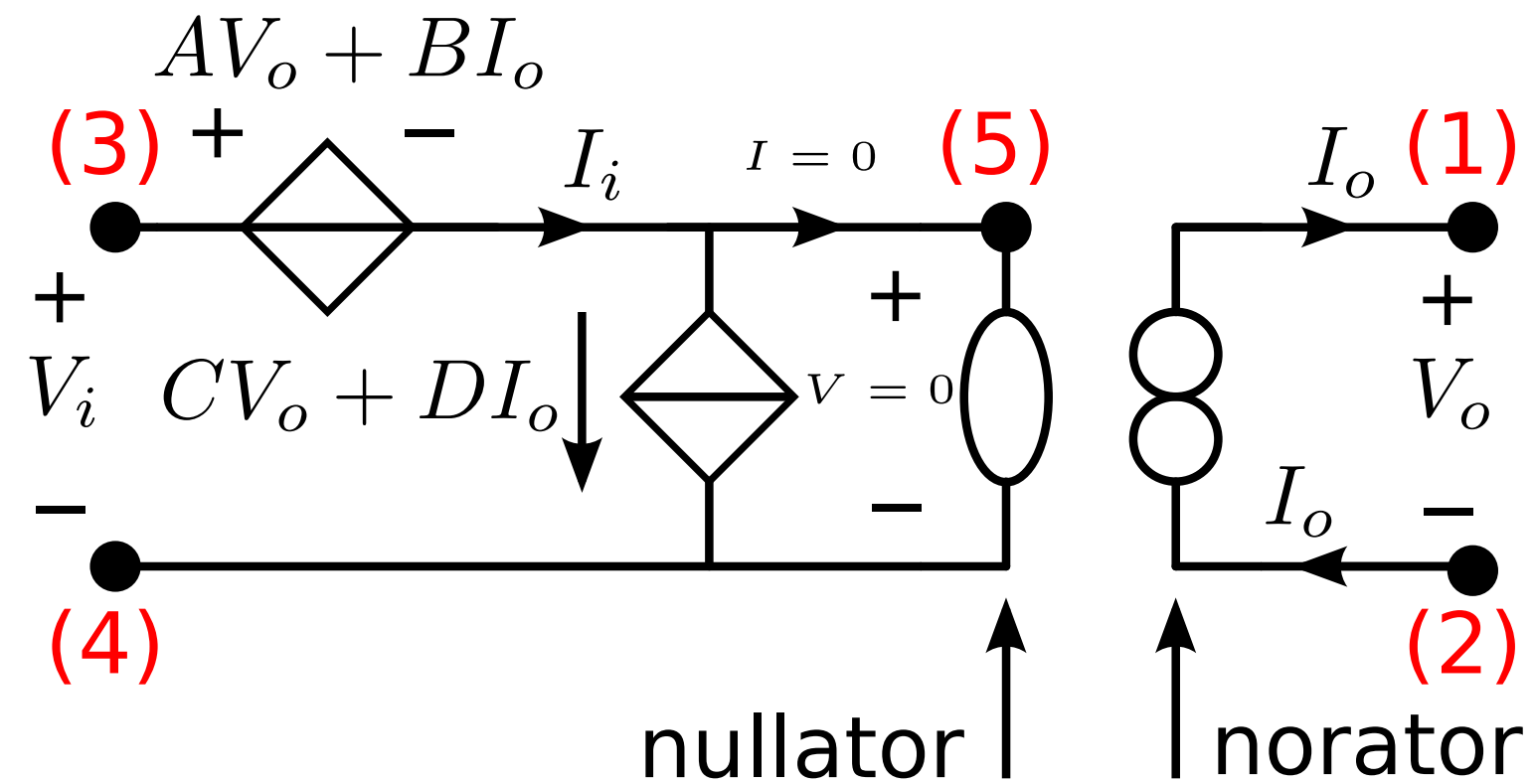
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Nullator and norator always  
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Nullator sets network condition

# Generalized two-port model



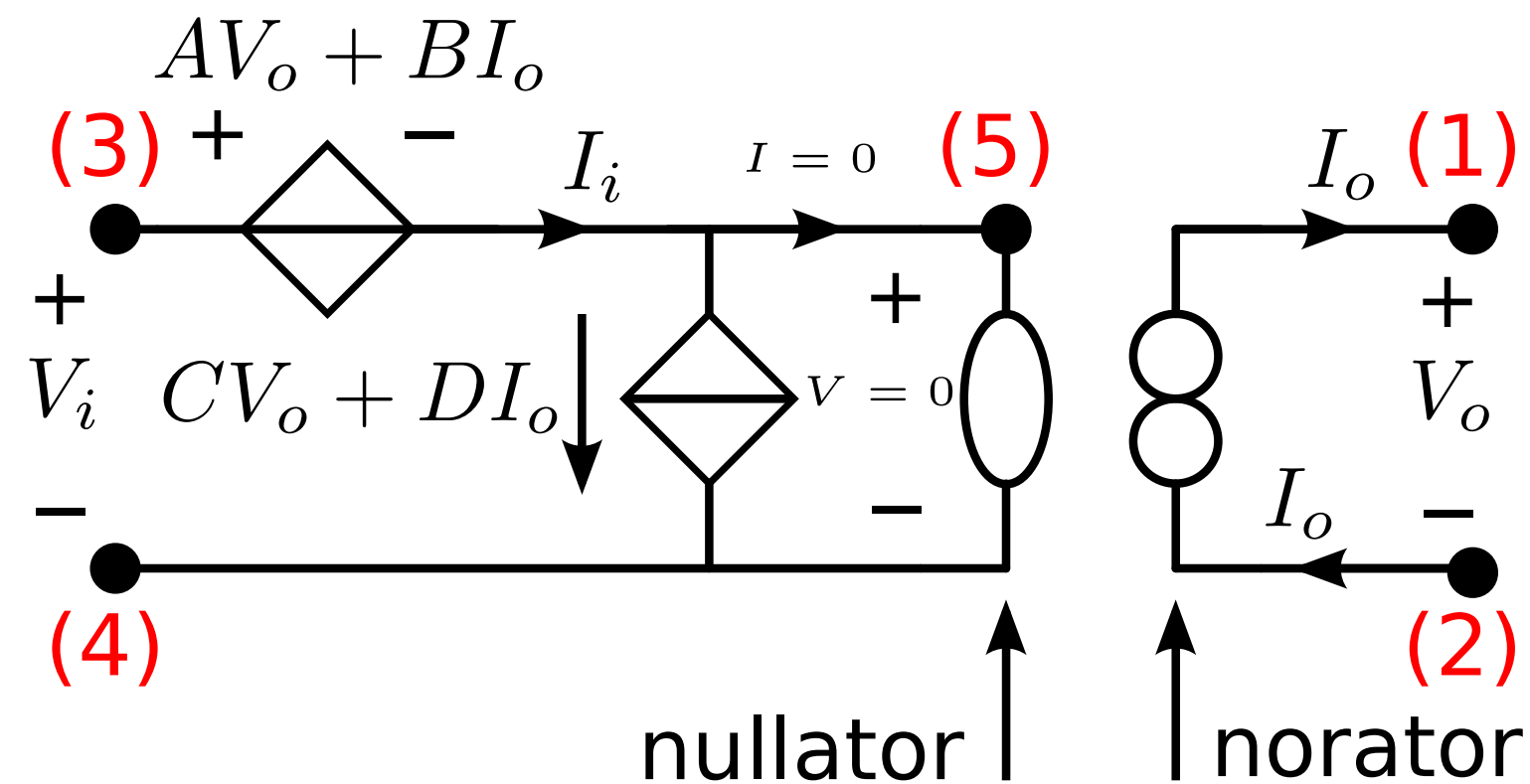
Nullator and norator always  
in pairs in a network  
See section 18.3.3

Nullator sets network condition

Norator adds variable



# Generalized two-port model

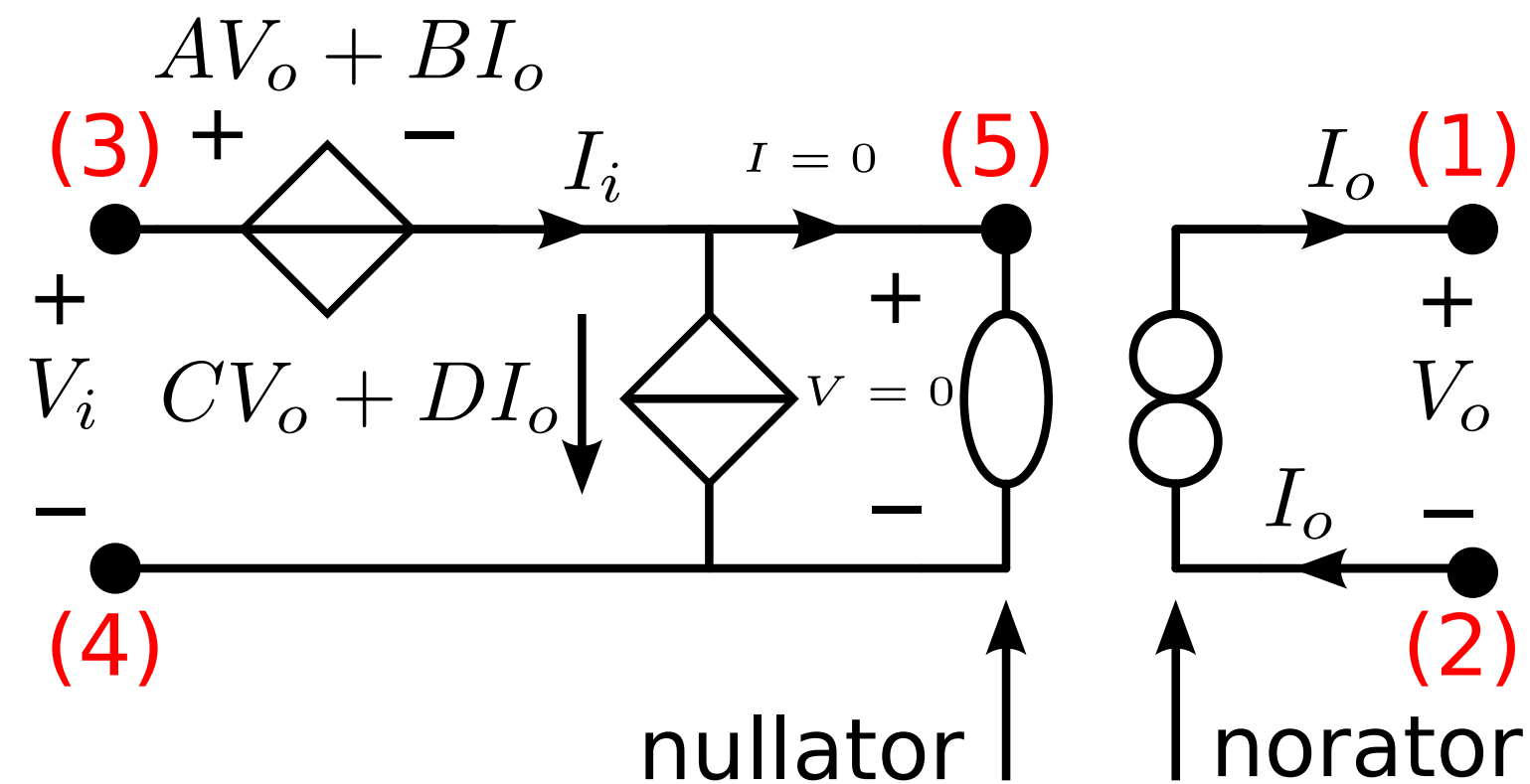


Nullator and norator always  
in pairs in a network  
See section 18.3.3

Nullator sets network condition  
Norator adds variable

Subcircuit included in SLiCAP: symbol SLABCD in LTspice.

# Generalized two-port model



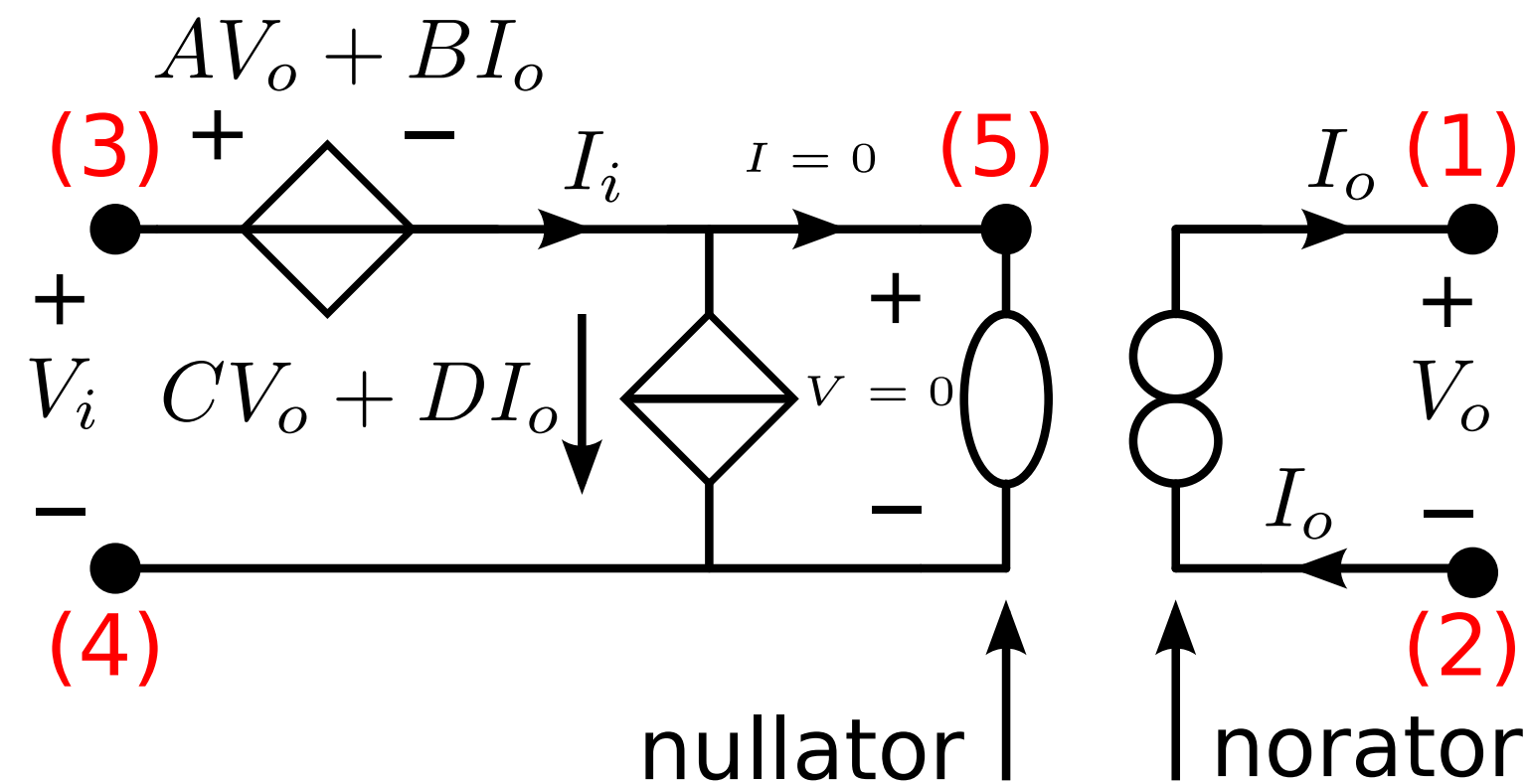
Nullator and norator always  
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Nullator sets network condition  
Norator adds variable

Subcircuit included in SLiCAP: symbol SLABCD in LTspice.

Can only be used with  $A, B, C, D = \text{Real}$

# Generalized two-port model



Nullator and norator always  
in pairs in a network  
See section 18.3.3

Nullator sets network condition  
Norator adds variable

Subcircuit included in SLiCAP: symbol SLABCD in LTspice.

Can only be used with  $A, B, C, D = \text{Real}$