

# Selected Topics from System modeling

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# Systems

Most physical systems show  
nonlinear, dynamic, time-variant  
and distributed behavior.

Their modeling, however, is to the  
convenience of the modeler.

G.P. Box: 'All models are wrong,  
but some are useful'.

*linear*  $\iff$  *nonlinear*

*instantaneous*  $\iff$  *dynamic*

*fixed*  $\iff$  *time – variant*

*causal*  $\iff$  *non – causal*

*stable*  $\iff$  *instable*

*lumped*  $\iff$  *distributed*

- Intended behavior of many information processing systems: linear, fixed, instantaneous, causal and stable
- Dynamic effects can be investigated by considering it linear
- Nonlinearity can be investigated by considering it instantaneous
- Nonlinear dynamic behavior can be modelled for special cases
- In this course only lumped systems

# Systems

Linear, instantaneous, fixed systems

- Input signal (excitation):  $x(t)$ , output signal (response)  $y(t)$ .
- Relation between response and excitation can be described with one constant  $G$ : system gain

$$y(t) = G \cdot x(t)$$

# Systems

Linear, dynamic, fixed systems

- Description with normal linear differential equations

$$\sum_{k=0}^{k=n} a_k \frac{d^k y(t)}{dt^k} = \sum_{i=0}^{i=m} b_i \frac{d^i x(t)}{dt^i}$$

- Coefficients are constants
- Solution with the aid of resolved signals
  - Time-domain: resolution in unit-impulse or unit-step functions, convolution
  - Frequency-domain modeling: resolution in imaginary exponentials: Cosine transform, Fourier series, Fourier Transform
  - Complex frequency-domain modeling: resolution into elementary complex exponentials: Laplace transform.

# Linear, dynamic, fixed system analysis

Modeling and analysis with time-domain resolved signals

## Modeling:

- Unit impulse response:  $\mathcal{H}\{\delta(t)\} = h(t)$
- Unit-step response:  $\mathcal{H}\{\mu(t)\} = a(t)$

## Analysis:

Convolution:

$$y(t) = h(t) * x(t) = \int_0^t h(t - \tau)x(\tau)d\tau$$

$$y(t) = a(t) * \dot{x}(t) = \int_0^t a(t - \tau)\dot{x}(\tau)d\tau$$

## Measurement:

Response to a periodic pulse can easily be related to unit-step response.

# Linear, dynamic, fixed systems

Modeling and analysis with frequency-domain resolved signals

- Uses resolution of pulse signals into imaginary exponentials
- Exponentials retain their shape under differentiation
- Differential equation is transformed into a power series in  $j\omega$ .
- Transfer function  $H(j\omega)$  relates the complex amplitude of component of the output signal to component of the excitation:

$$H(j\omega) = \frac{Y(j\omega)}{X(j\omega)}, \quad H(j\omega) = \mathcal{F} \{h(t)\}$$

$$\frac{S_y(\omega)}{S_x(\omega)} = |H(j\omega)|^2$$

# Linear, dynamic, fixed systems

Modeling and analysis with complex frequency-domain resolved signals

- Uses resolution of signals into complex exponentials
- Exponentials retain their shape under differentiation
- Differential equation is transformed into a power series in  $s$ .
- System function  $H(s)$  relates the complex amplitude of one component of the output signal to the corresponding component of the excitation:

$$Y(s) = H(s)X(s), \quad H(s) = \mathcal{L}\{h(t)\}$$

- Time domain analysis using Laplace:

$$y(t) = \mathcal{L}^{-1}\{Y(s)\} = \mathcal{L}^{-1}\{H(s)X(s)\} = \mathcal{L}^{-1}[H(s)\mathcal{L}\{x(t)\}]$$

# Linear, dynamic, fixed systems

Fourier versus Laplace

- Both transformation methods can be used for solving linear time invariant differential equations
- Fourier: all signals must be absolute integrable:

$$\int_{-\infty}^{\infty} |x(t)| dt < \infty$$

- Cannot be used for instable systems with theoretically unbounded response to bounded input



# Linear, dynamic, fixed systems

## Characterization of the system function

System function  $H(s)$ ;  $a_k$  and  $b_i$  coefficients of differential equation:

$$H(s) = \frac{Y(s)}{X(s)} = \frac{\sum_{i=0}^{m} b_i s^i}{\sum_{k=0}^n a_k s^k}$$

Characterization with poles and zeros:

$$H(s) = \frac{b_0}{a_0} \frac{\prod_{i=1}^m (1 - s/z_i)}{\prod_{k=1}^n (1 - s/p_k)} \quad \text{or} \quad H(s) = \frac{b_m}{a_n} \frac{\prod_{i=0}^{m-1} (s - z_i)}{\prod_{k=0}^{n-1} (s - p_k)}$$

Zero frequency transfer  $H(0)$  if  $a_0 \neq 0$ , :  $H(0) = \frac{b_0}{a_0}$

Transfer for  $s \rightarrow \infty$ , ( $n > m$ ) :  $H(s)_{s \rightarrow \infty} = \frac{b_m}{a_n s^{n-m}}$

# Linear, dynamic, fixed systems

## Impulse response

- ① System has  $k$  poles, of which  $\ell$  different (non coinciding)
- ② A pole  $p_\ell$  occurs  $q$  times

$$h(t) = \sum_{i=1}^{\ell} \left( \sum_{j=1}^q \frac{A_j}{(j-1)!} t^{j-1} \exp p_\ell t \right)$$

- ③  $A_j$  follows from partial fraction expansion (residues)

Stable if  $\text{Re}(p_\ell) < 0$  for all  $\ell$ ; poles in left half of  $s$  - plane.

# Linear, dynamic, fixed systems

Relations between description methods

## Relation between pole-zero diagram and step response

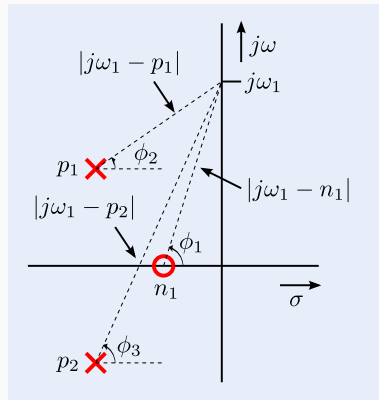
- Laplace transform of unit step:  $\mathcal{L}\{\mu(t)\} = \frac{1}{s}$
- Laplace transform of the unit impulse is the system function  $H(s)$
- Unit step response :  $a(t)$
- Initial value theorem:  $a(0^+) = \lim_{s \rightarrow \infty} s \frac{1}{s} H(s) = \lim_{s \rightarrow \infty} H(s)$
- Final value theorem:  $a(\infty) = \lim_{s \rightarrow 0} s \frac{1}{s} H(s) = \lim_{s \rightarrow 0} H(s)$

# Linear, dynamic, fixed systems

## Relations between description methods

Relation between pole-zero  
diagram and Bode Plots:  
 $s = j\omega$ .

$$H(j\omega) = \frac{b_m}{a_n} \frac{\prod_{i=0}^{m-1} (j\omega - z_i)}{\prod_{k=0}^{n-1} (j\omega - p_k)}$$



# System modeling

Nonlinear, instantaneous, fixed systems

- Modeling with the aid of Taylor series
- Instantaneous behavior = frequency-independent behavior
- Characterization: various description methods for deviation from linear behavior exist.
- Description methods that closely relate to the observer's error perception, should be used.
- Offset
- Gain
- Nonlinearity
- Differential-gain
- Harmonic distortion
- Intermodulation distortion
- Gain compression

# Nonlinear instantaneous fixed

Description with Taylor series

Taylor expansion in origin of a static nonlinear function  $y(x)$  :

$$y(x) = a_0 + a_1x + a_2x^2 + \dots a_nx^n$$

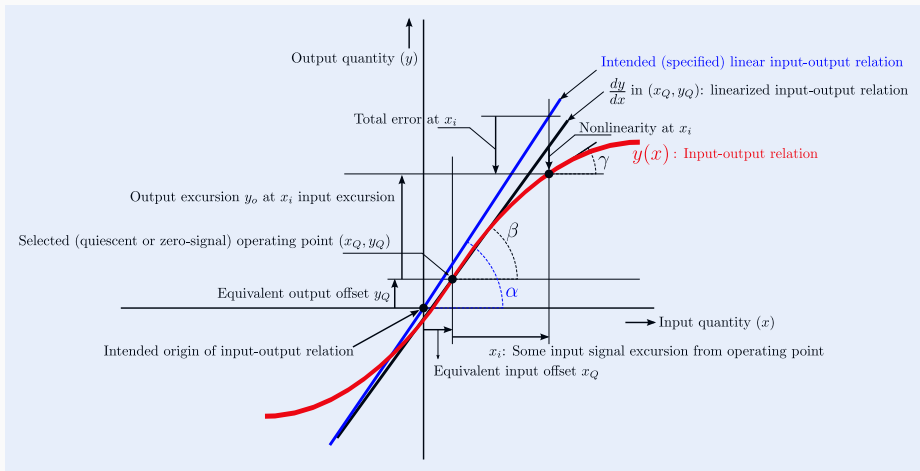
$$a_n = \frac{1}{n!} \frac{d^n y}{dx^n}$$

$a_0$  : offset

$a_1$  : gain

# Nonlinear instantaneous fixed

## Static input-output relation



# Nonlinear instantaneous fixed

## Harmonic and intermodulation distortion

- Higher order terms from Taylor series cause offset, harmonic distortion and intermodulation distortion:

$$\cos^2 \omega t = \frac{1}{2} + \frac{1}{2} \cos 2\omega t$$

$$\begin{aligned} (\cos \omega_1 t + \cos \omega_2 t)^2 &= \cos^2 \omega_1 t + \cos^2 \omega_2 t + \\ &+ \cos (\omega_1 - \omega_2) t + \cos (\omega_1 + \omega_2) t \end{aligned}$$

- Total harmonic distortion (THD): ratio of the power of all harmonics and of the fundamental
- Intermodulation distortion (IMD), two fundamentals with equal amplitude: ratio of the power of the intermodulation component and that of one fundamental. Second order IMD:  $\omega_1 \pm \omega_2$ , third-order IMD  $2\omega_1 \pm \omega_2$  or  $\omega_1 \pm 2\omega_2$  etc.



# Nonlinear instantaneous fixed

## Harmonic and intermodulation distortion and differential gain

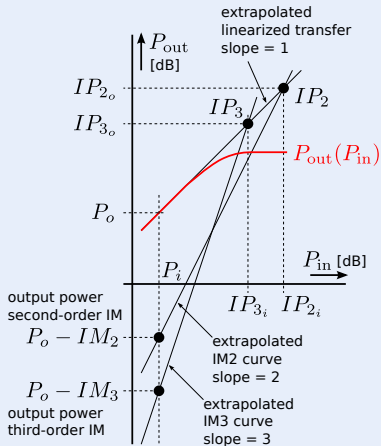
For instantaneous fixed nonlinear systems there exists a relation between the harmonic and intermodulation distortion and the differential gain:

$$d_2 = \frac{\varepsilon^+ - \varepsilon^-}{8}, \quad d_3 = \frac{\varepsilon^+ + \varepsilon^-}{24}$$
$$IM_2 = \frac{\varepsilon^+ - \varepsilon^-}{4}, \quad IM_3 = \frac{\varepsilon^+ + \varepsilon^-}{8}$$

$\varepsilon^+$  and  $\varepsilon^-$  are the differential gain at positive and negative peak excursion (considering one carrier for IMD), respectively.

# Nonlinear instantaneous fixed

## Intermodulation intercept points



# System modeling

Nonlinear, dynamic, fixed systems

- ① Differential-gain: depends on frequency
- ② Differential phase: depend on frequency
- ③ THD: depend on frequency; relations between the differential gain and the second and third order harmonic distortion are not longer valid.
- ④ Intermodulation: depends on frequency; relations between the differential gain and the second and third order intermodulation distortion are not longer valid.
- ⑤ Gain compression: depends on frequency; relation between the IP3 and the 1 [dB] compression point is not longer valid.
- ⑥ Slew rate limitation:

$$SR^+ = \left. \frac{dy(t)}{dt} \right|_{\max} ; \text{ if } \frac{dy(t)}{dt} \geq 0$$
$$SR^- = - \left| \left. \frac{dy(t)}{dt} \right|_{\max} \right| ; \text{ if } \frac{dy(t)}{dt} < 0$$

# Slew rate and full-power bandwidth

Limiting and dynamic effects

- Limiting voltage with inductive load causes a limited rate of change of the current:

$$\left. \frac{di}{dt} \right|_{\max} = \frac{V_{\max}}{L}$$

- Limiting current with capacitive load causes a limited rate of change of the current:

$$\left. \frac{dv}{dt} \right|_{\max} = \frac{I_{\max}}{C}$$

- Full-power bandwidth: maximum frequency at which no slew-rate distortion can be observed, at a given amplitude of a sinusoidal output signal.